FINAL REPORT

Brice Ohl

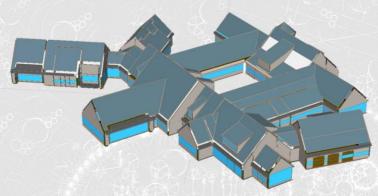
Mechanical Option

Advisor Professor Stephen Treado

Submitted 4.3.2012

The New Offices for RLPS Architects

Lancaster, PA



Brice Ohl | Mechanical Option | The New Office Building for RLPS Architects | Lancaster PA

www.engr.psu.edu/ae/thesis/portfolios/2013/beo107/index.htm

+Building Statistics

Number of Stories: 1 Full ground level with mezzanine level. The mezzanine includes a small storage area and a larger area that acts as a mechanical and electrical space over a large portion of the ground level.

Total Size: 22,500 SF

Project Cost: \$1,000,000 Electrical, \$900,000 Mechanical, \$440,000 Plumbing + Fire Protection

+Mechanical Systems

The New Office Building will be utilizing a geothermal well system of 8 loops. The well system will be managed and pumped from a ground level mechanical space, while the spaces will be conditioned from terminal units typically placed in a mechanical mezzanine.



The left image is an example of the catwalk common in the mezzanine. The right image is heat pump group for a wing.

+Lighting Electrical Systems

Electrical service will be provided a new PPL Transformer sized for 300 kVA. Service to all of the panels will be 3 phase, 4 wires, and 120/208V. The artificial lighting was designed for energy efficiency and incorporates dimming schedules and occupancy sensors.





The left image shows the new transformer outside of the ground level mechanical room. The right image shows the primary distribution center in that room.

+Structure

The new office building primarily utilizes a wooden structure with some small uses of load bearing walls of block construction. The mezzanine space created by the roof frame was designed not only for structural integrity, but also houses space for MEP equipment and access via catwalks throughout most of the building.



The left image is an example of exposed structure while the right image is an example of unexposed structure in the mezzanine.

+Architecture

The site of the building is primarily independent, but is situated in a more residential area. The new office has some styles of a colonial home, but with a modern feel. One focus is an interior courtyard with water feature that is visible from all of the studio spaces.



The left image is the main entrance for employees. The right image shows the lobby and main business entrance.

+Project Team

Owner Architects General Contractor RLPS Architects RLPS Architects Warfel Construction

Mechanical Engineers
Electrical Engineers
Structural Engineers

Reese Engineering Inc. Reese Engineering Inc. Zug & Associates, Ltd.

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Executive Summary

The objective of this report is to review the possible implementation of a hybrid ventilation system focused around the buildings courtyard.

The first option was to use automated windows between the work spaces and the courtyard to allow additional outdoor air into the office building. The idea was that the temperate climate of Lancaster, Pa would provide some chances to reduce energy consumption by using outdoor air.

The second option was more of an addition to the first. There already exists a water feature in the courtyard. The second option was to use water feature (likely a different one) as an air cleaner to normalize the air quality of the courtyard. To aid the water feature grey water would be collected and stored in a subgrade cistern until it achieved ground temperature. Once it reaches ground temperature the water would be pumped to the water feature.

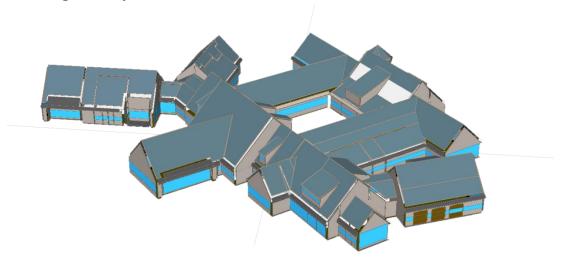
Ina addition to mechanical changes the effects of the system on the electrical system and construction costs were considered. It was found the system could be easily implemented into the buildings electrical systems. However, the construction costs reached an estimated \$261,479.

The cost of the construction of the hybrid system, in the proposed fashion proved to be too high. The generally accepted payback period range of 3 to 5 five years was far exceeded.

The final recommendation of this report was to not implement the proposed system, but to consider a less automated system that relies on the occupants and operable windows.

Building Overview

Building Description



The New Office Building for RLPS Architects is a new construction office building located in Lancaster County, PA. It totals 22,500 square feet which is split between one full ground level and a small mezzanine area, to be used for storage. The use of this building is primarily office spaces, studio space, or group work areas. Some unique features to the building include a bistro area and adjoined living room space. Additionally, there is an interior courtyard complete with a water feature. Overall, the building is classified as Business with an occupancy capacity just short of 230 people. The expected completion date is January 2013.

Architecture

The site of the building is primarily independent, but is situated in a more residential area. The new office has some styles of a colonial home, but with a modern feel. One focus is an interior courtyard with water feature that is visible from all of the studio spaces.

Occupant and Project Team

Owner & Architects: RLPS Architects Ltd.
General Contractor: Warfel Construction

Mechanical & Electrical Engineers: Reese Engineering Inc.

Structural Engineers: Zug & Associates, Ltd. Structural Engineers.

Civil Engineers: Harbor Engineering

Surveyor: Herbert, Rowland, & Grubic, Inc.

Landscaping: RLPS Architects Ltd.

Mechanical System Overview

1.1 Mechanical System Design Layout

Though the new office building covers just above 22,000 square feet the design is spread out which limited the ability to use a primary air handling unit. To reduce pressure losses by using extensive duct work as well as to save on the space used terminal units were used for each space. Additionally, spaces were grouped in areas designated by a letter.

Figure 1 below depicts the site orientation as well as the area designations used by the project engineer. These areas will be referenced throughout the report.

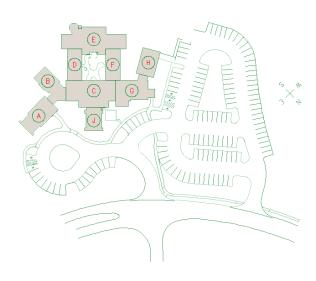


Figure 1

The primary mechanical space is on the ground level in Area G. The mechanical mezzanine that houses most of the terminal units can be entered through a storage mezzanine in Area H. The mechanical mezzanine spreads from Area H through Areas A, B, C, J, and G. Area E has a separate mechanical mezzanine that houses the ventilation units for the entire building.

Images 2 and 3 depicting the ground level mechanical space and the mechanical mezzanine areas can be found in Appendix A.

1.2 Mechanical System Air Supply Design

The air side design of the new office building is relatively simple. There are 28 water source heat pump terminal units spread throughout the building to serve mostly individual spaces. All of them save one are placed in mechanical mezzanines usually in groups of five to eight. The one terminal unit not in the mechanical mezzanine is in a ground level closet in Area C. The terminal units provide both heating and cooling capacities. These capacities vary per unit as well as the air volume flow rate which ranges from 300 CFM to 1800 CFM. The terminal units use electricity as the primary fuel source, running at 208/1/60, but varying in maximum amperage capacity with each unit.

The outdoor air is provided to the building by 4 ventilation units situated in the Area E mechanical mezzanine. These ventilation units provide the air to the various pods of terminal units through ductwork above the acoustical ceilings in the Area F and Area D.

Exhaust fans are also Part of the airside design. Due to the nature of the work being done in the new office building little exhaust is needed. However, a few spaces require localized exhaust, these areas include the restrooms, the ground level mechanical space, and the printing area.

1.3 Mechanical System Hydronic Design

The hydronic systems for the new office building are also a relatively simple process. The unique feature is the ground source well system. The well system consists of 8 closed loops that run beneath the parking lot. The loops enter the building under the carriage house doors in Area H and head to the ground level mechanical space in Area G. The pump that drives the conditioned water rests in the Area G mechanical space. There are two pumps with 300 GPM capacities. The second is a backup pump; there are mechanisms in place to prevent the pumps from running simultaneously. From the mechanical space the conditioned water is pumped to the individual terminal units where it exchanges heat. The water then circulates back through the mechanical space. To maintain regular pressure the heat pump loop also includes an expansion tank with a 80 gallon capacity.

Additionally, for cases of cooling conditions there are condensate lines and small pump with 3 GPM capacity that return condensate to the ground level mechanical space.

Figure 4 in Appendix A, depicts the well field situated below the parking lot.

Figure 5 IN Appendix A, depicts the general setup of the ground source loop as described above.

1.4 Mechanical System Modeled Performance

In addition to the physical layout of the mechanical system the performance must also be considered. Figure 6 below is a table depicting the modeled performance of the current building design with not hybrid implementations. The building was modeled using Carrier Corporation's Hourly Analysis Program version 4.6.

	Modeled (HAP v4.6)
Cooling [tons]	47.0
Cooling [sf/ton]	460
Cooling [cfm/ton]	N/A
Cooling [Btuh/sf]	26.1
Heating [Btuh/sf]	21.0
Design air Flow [cfm]	29336
Supply [cfm/sf]	1.36

Figure 6

The table below, Figure 7, is an analysis of the cost for running the various mechanical pieces per annum. The final column shows that the new office building relatively consistent with the national average for office buildings.

HVAC	Cost [\$/yr]	Cost per area	Percent of Total Cost	National Avg. for
Components		[\$/sf]	[%]	Office Buildings [%]
Air System Fan	2,274	0.105	7.1	5
Cooling	3,829	0.177	12.0	9
Heating	3,585	0.166	11.2	25
Pumps	3,765	0.174	11.8	N/A
Non-HVAC				
Components				
Lights	8,679	0.402	27.2	29
Electrical	9,803	0.454	30.7	16
Equipment				
Total	31,931	1.477	100	

Figure 7

The final performance table, Figure **8**, displays the modeled emissions for the new office building. All fo the values were tested and found to be acceptable. The proposed system will unlikely reduce emissions on site unless a water sprayer configuration was selected for the water feature. The water sprayer could remove particulate matter. Otherwise the emission reductions would be offsite at the plant providing electric power due to the reduction of electrical power consumption.

Pollutant	[lb of pollutant per kWh]	[lb pollutant/year]
CO2	1.64	1.81x10 ⁵
NOx	3.0x10 ⁻³	3316
SOx	8.57x10 ⁻³	9474
Particulate Matter	9.26x10 ⁻⁵	102

Figure 8

1.5 LEED 2009 Analysis

A LEED 2009 evaluation was performed for this project. The LEED 2009 Project checklist for New Construction. Since the project owner has not specified a level of LEED achievement yet, it was assumed that basic LEED certification was the only requirement. Let it be noted that only points that could be confirmed in the project specifications or project teams' sustainability discussions were awarded. The project has the ability to earn more credits than the ones listed below, but has not indicated a definite attempt at the other credits.

The following tables makeup the evaluation of LEED 2009 certification. The 'intent' of each credit is directly from the USGBC.

Sustainable Sites	Points: 7/26	
Credit	Action	Points
SS Prerequisite 1: Construction Activity Pollution		N/A
Prevention		
Intent. To value and listing frame construction		
Intent: To reduce pollution from construction		
activities by controlling soil erosion, waterway		
sedimentation and airborne dust generation.	67 1 11 11	_
SS Credit 2: Development of Density and	Option 2: The new office building is	5
Community Connectivity	located across the street from a	
	residential neighborhood. Additionally, it	
Intent: To channel development to urban areas	provides pedestrian access to the	
with existing infrastructure, protect greenfields,	Oregon Pike and a great number of basic	
and preserve habitat and natural resources.	services.	
SS Credit 8: Light Pollution Reduction	Option 1: Non-essential interior lighting	1
	has been designed for automatic lighting	
Intent: To minimize light trespass from the	control.	
building and site, reduce sky-glow to increase	The exterior lighting has a simulated	
night sky access, improve nighttime visibility	power density of 0.056 [W/SF] which is	
through the glare reduction and reduce	below the LEED allowable of 0.12	
development impact from lighting on nocturnal	[W/SF].	
environments.	[, -]	

Water Efficiency	Points: 5/10	
Credit	Action	Points
WE Prerequisite 1: Water Use Reduction		N/A
Intent: To reduce pollution from construction activities by controlling soil erosion, waterway sedimentation and airborne dust generation.		
WE Credit 2: Innovative Wastewater Technologies Intent: To reduce wastewater generation and potable water demand while increasing the local aquifer recharge.	The utilization of dual flush water closets has lowered the water consumption of the new office building. Additionally, an estimated 75,777 gallons of rain water reuse helped qualify the building for 2 points.	2
WE Credit 3: Water Use Reduction Intent: To further increase water efficiency within buildings to reduce burden on municipal water supply and wastewater systems.	High efficiency fixtures were selected across the building. Current calculations by the project engineer indicate a 36% water savings, which is more than the required 35% for 3 points.	3

Energy & Atmosphere	Poin	ts:7/35
Credit	Action	Points
EA Prerequisite 1: Fundamental Commissioning		N/A
of Building Energy Systems		
Intent: To verify that the project's energy-related		
systems are installed, and calibrated to perform		
according to the owner's project requirements,		
basis of design and construction documents.		NI/A
EA Prerequisite 2: Minimum Energy Performance		N/A
Intent: To establish the minimum level of energy		
efficiency for the proposed building and systems		
to reduce the environmental and economic		
impacts associated with excessive energy use.		
EA Prerequisite 3: Fundamental Refrigerant		N/A
Management		
Intent: To reduce stratospheric ozone depletion.		
EA Credit 1: Optimize Energy Performance	The design engineer use the	5/10
	Performance Rating Method, defined by	
Intent: To achieve increasing levels of energy	ASHRAE 90.1-2004, accepted by LEED	
performance beyond the prerequisite standard	to calculate predicted energy	
to reduce environmental and economic impacts	performance.	
associated with excessive energy use. EA Credit 4: Enhanced Refrigerant Management	Option 2: The heat pumps selected were	2
LA Oreuit 4. Lillianceu Nemgerant Management	also selected with a refrigerant	_
Intent: To reduce ozone depletion and support	management provisions. The overall	
early compliance with the Montreal Protocol	refrigerant impact per ton is 71.6, less	
while minimizing direct contributions to climate	than the maximum 100 for the credit.	
change.	2.5 2.5	

Materials & Resources	Points: xx/14	
Credit	Action	Points
MR Prerequisite 1: Storage and Collection of		N/A
Recyclables		
Intent: To facilitate the reduction of waste generated by building occupants that is hauled to and disposed of in landfills.		

Indoor Environmental Quality	Point	s: 5/15
Credit	Action	Points
IEQ Prerequisite 1: Minimum Indoor Air Quality Performance		N/A
Intent: To prevent or minimize exposure of building occupants, indoor surfaces and ventilation air distribution systems to environmental tobacco smoke (ETS).		
IEQ Prerequisite 2: Environmental Tobacco Smoke (ETS) Control		N/A
Intent: To establish the minimum level of energy efficiency for the proposed building and systems to reduce the environmental and economic impacts associated with excessive energy use.		
IEQ Credit 1: Outdoor Air Delivery Monitoring Intent: To provide capacity for ventilation system	CO2 monitoring is fitted in all ventilation systems, and report to the system BAS.	1
monitoring to help promote occupant comfort and well-being.		
IEQ Credit 2: Increased Ventilation	Option 1: All zones and terminal units were designed and sized to exceed	1
Intent: To provide additional outdoor air ventilation to improve indoor air quality (IAQ) and promote occupant comfort, well-being and productivity.	minimum outdoor air by at least 30%. Supporting documentation was provided.	
IEQ Credit 6.1: Controllability of Systems – Thermal Comfort	80 of the 81 individual workspaces will be outfitted with lighting controls and occupancy sensors. The control options	1
Intent: To provide high level of thermal comfort system control by individual occupants or groups in multi-occupant spaces and promote their productivity, comfort and well-being.	include dimming and dual level switching	

IEQ Credit 6.2: Outdoor Air Delivery Monitoring Intent: To provide capacity for ventilation system monitoring to help promote occupant comfort and well-being.	The specifications call for a number of full color display units to both monitor and control the BAS. The system qualifies for multi-occupant space comfort control.	1
IEQ Credit 7.1: Outdoor Air Delivery Monitoring Intent: To provide comfortable thermal environment that promotes occupant productivity and well-being.	The system design utilizes the four ventilation units for outdoor air, the units have the ability to regulate temperature and humidity appropriately.	1

The current 19 awarded credits is insufficient for LEED Certification. Remember though that LEED is not yet a goal for the owner. Also there are a number of points that could be awarded (especially in the Materials & Resources Category) that only need further documentation or verification upon construction completion.

Proposed Mechanical Redesign

1.1 Hybrid Ventilation

The primary proposal for the mechanical system was to integrate a hybrid ventilation system. This was chosen as documentation shows that both the owners and the design team were striving for a very efficient building. Additionally, the existing ground source well system has already increased the 'plant' side if the system. The hybrid ventilation was selected in hopes to improve the air delivery aspects of the mechanical systems.

The proposed design centers around the interior courtyard between Area C, Area D, Area E, and Area F. The proposed redesign was to change the Area D and Area F walls that encompass the from primarily glass panels to partitions of automated windows. The window automation would allow for outdoor air to enter the work spaces under proper weather conditions lowering the heating and cooling loads for the terminal units.

1.2 Hybrid Ventilation with Grey Water Reuse

An additional test to the implementation of a hybrid ventilation system centered around the water feature within the interior courtyard. It was proposed to use the water feature as a means of extending the possible hybrid ventilation by focusing the outdoor temperatures towards more acceptable indoor temperatures. This would be achieved by collecting grey water in a subgrade cistern where it may sit as its temperature normalizes to ground temperature much like a ground source well field. This grey water would be filtered and pumped to the water feature where is would act as an air cleaner. The goal is for the water feature to normalize the air temperature and humidity.

Proposed Electrical Breadth Study

1.1 Additional Electrical Load

With the addition of the devices required for window automation there will be an additional load that was not accounted for in the original electrical design. The number and nature of these devices will calculated and discovered. Furthermore, the additional electrical load will possibly be integrated into the existing system.

1.2 Electrical System Reconfiguration

With the addition of the window automation electrical load it was proposed that the electrical systems could be reconfigured to accommodate this. Additionally, at times of hybrid ventilation the electrical consumptions could drop substantially, possibly allowing for reducing some electrical systems.

Proposed Construction Breadth Study

1.1 Additional Cost Estimate

The implementation of the hybrid system would obviously require additional pieces raising the construction cost. These pieces range from the grey water collection system part to the window automation devices. Moreover, there will be a need for further excavation than previously planned to place the grey water cistern below grade. All of these items will be considered for the new construction cost.

1.2 Additional Construction Time

In addition to construction cost, the time required for the additional construction was considered to ensure that the overall construction time of the building would not be extended in any great way. From the outlook the cistern placement could pose as a problem to the schedule as one must be ordered well in advance to its placement date. Additionally, the cistern will require unplanned excavation. This excavation will be away from the current design floor plan, but is a concern.

Mechanical System Redesign Methods

1.1 Weather Data

Weather data was acquired from the Trane Inc. program Trace 700. This weather data was used to find the typical outdoor conditions for each hour of the day for a standard day of each month. Based off of given dry bulb and wet bulb conditions the relative humidity, absolute humidity, and air density could be solved for using psychrometric charts.

1.2 Air Mixing Methods

To find under what conditions outdoor air could be used to the maximum, but still maintain acceptable indoor conditions. To do this air mixes were considered at 10% outdoor air intervals, starting with minimum outdoor air then proceeding to 10% outdoor air, 20% outdoor air, etc. The primary goal was to the mixed air temperature and the mixed air relative humidity to make sure it fell within acceptable ranges set forth by ASHRAE.

The temperature mixing equation used is described below:

The process for solving for the mixed air relative humidity was slightly more difficult. Instead of one step it involved two. The first was to solve for the absolute humidity of the mix. The second step was to use psychrometric charts to find the relative humidity of the mix based of the absolute humidity and dry bulb temperature.

The absolute humidity mixing equation used is described below:

$$W_{Mix} = W_{Outdoor} + (\dot{m}_{Heat Pump} / \dot{m}_{Total}) (W_{Heat Pump} - W_{Outdoor})$$

W is the absolute humidity, \dot{m} is calculated from the volume flow rate and the air density for the given conditions. The values from the heat pump were taken from design documents and schedules.

1.3 Mixing Method Testing

To test if a particular air mixture would successfully yield acceptable temperature and humidity conditions logic functions were used in Microsoft Excel. The functions tested if the minimum design temperatures were met and the maximum design temperatures were not exceeded. The same was performed for the relative humidity. If a particular setup (E.G. Hour 2 of January at 50% Outdoor Air) was found acceptable it would be added to the total hours of hybrid ventilation at 50% outdoor air.

The tables designed and used to calculate the hybrid ventilation are in Appendix B: Hybrid Ventilation Calculations and Results.

Mechanical System Redesign Results

1.1 Assumptions for Results in Standard Conditions

To model the possible hybrid ventilation time there were several assumptions that needed to be made. These assumptions were made both within the calculations, about the physical setup of the space, and how the air was mixed.

One of the largest assumptions is that the outdoor air and the forced air will mix perfectly. This is assumed for both the mixed temperature and the mixed relative humidity. Additionally, it was assumed that the outdoor air temperature in constant within the interior courtyard. The wall between the courtyard and Area F has a stationary trellis that had it shading coefficient omitted from the calculations. Finally, the calculations were performed using the design air flow rate for the entire building. It was assumed that the mixed outdoor and forced air would spread from the areas surrounding the courtyard freely to all spaces within the building.

1.2 Results of Calculated Hybrid Time for Standard Conditions

The results of the calculated hybrid ventilation time are promising. They yield that up to 7% of all of the hours in the year 100% outdoor air could be used. As you would expect the amount of time that the various outdoor air levels can run increases as you approach the minimum rates.



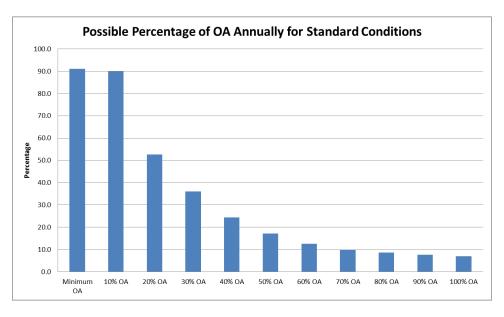


Figure 9

Figure XX in appendix A shows the complete results for the standard conditions. This includes the number of hours achievable for each outdoor air margin for both winter design conditions, summer design conditions and a combination of both.

1.3 Assumptions for Results in Water Feature Conditions

The model for hybrid conditions combined with the water feature included the same assumptions as the model for standard conditions. However, the modeling of the water feature's results also came with some new assumptions. Firstly, there were two water feature models considered. The first option modeled the water feature as a water spraying air cleaner. This was the first choice as it would not only provide air conditioning, but also help remove particulate matter. The second option modeled the water feature as a constant temperature surface that the air could primarily have convective heat transfer with. Interestingly both models yielded similar results. For the sake of brevity, this report reflects the first option.

The assumptions made to model the air cleaner include that it would be at %60 efficiency. Standard air cleaners range from 60% to 80%. Given that the 'air cleaner' would in open conditions it was assumed to be on the low end of efficiency.

1.4 Results of Calculated Hybrid Time for Water Feature Conditions

The results for the water feature conditions were somewhat surprising. In the minimum to 40% outdoor air margin range the water feature did increase the number of hours possible to run hybrid ventilation. However when trying to achieve 50% outdoor air or above the water feature decreases the number of hours minutely.



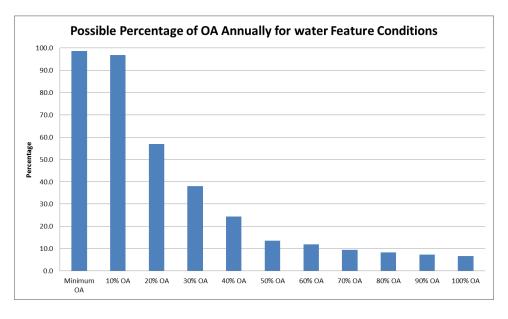


Figure 10

Figure 10 depicts the percentage of hours that each outdoor air margin can meet for both standard conditions and water feature conditions.

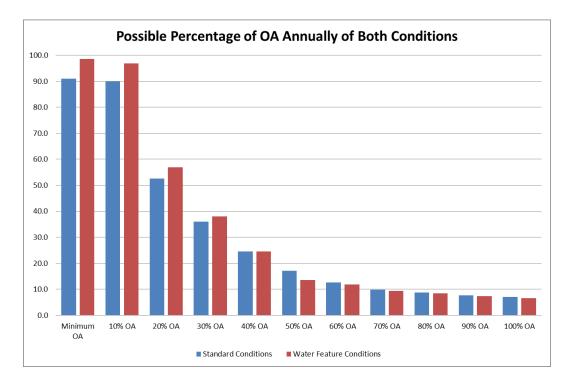


Figure 10

For a comparison of total hours for each condition search Figure 11 Appendix A.

1.5 Estimated Energy Savings from Hybrid Ventilation

The ultimate goal of the hybrid ventilation system is to save on heating and cooling loads. This will in turn lower the energy consumption of the building. Figure 12 below is a table showing the estimated energy savings that the hybrid system would provide. These values are on the extreme end of efficiency. They were calculated as thought the hybrid system was always running at the peak outdoor air rate. Additionally, these calculations were based on a typical hour for each hour of each month. This does not account for poor weather or atypical weather. Finally, due to the heat pumps that were being used having such a variety the energy consumption was calculated linearly with the outdoor air use (E.G. 0% outdoor air correlates to 100% energy consumption and 100% outdoor air correlates to 0% energy consumption.) Because this is not an actuality, correction factors were use.

Components	Current System Energy Use [kWh]	Energy Use with Hybrid Ventilation [kWh]	[%] of Current System
Cooling Coil	34919	27351	78.3
Compressor			
Heating Coil	32717	28496	87.1
Compressor			
Terminal Fan	20751	15296	73.7
Compressor			
Total	88387	71143	80

Figure 12

With the calculated energy savings of about 20% and the cost of electricity [\$ 0.10346] the annual savings could be up \$1,784 annually. This cost savings would likely not prove this proposal a viable option. The hopeful payback period is within 3 to 5 years, this leaves little room for the construction costs.

Electrical Breadth Analysis

1.1 Additional Electrical Load

The addition of the automated windows did add several electronic devices that the original electrical design did not call for. The basic pieces of a window automation and control system are actuator packages, motor controller, outstation controller, temperature sensors, humidity sensors, and CO_2 sensors. The actuator package is the device that physically opens the window by extending an actuator and closing the window via chain. The motor controller acts as a central control unit that receives the outdoor conditions and signals the actuators to open or close the window. The outstation controller is the device that the user can interface with, normally via a touchscreen. Select outstation controller can also be connected to building BAS systems. Temperature, humidity, and CO2 sensors are self-explanatory, but let it be noted that they can made in combination.

These devices can come in a variety of sizes, configurations, and names. The nomenclature this report uses was found to be common amongst several manufacturers. In addition to nomenclature and configurations these devices can vary in electrical consumption. The values used for this report were found to be typical or averaged among several manufacturers.

Moreover the quantity of devices needed rely on each other. For example a typical motor controller can handle six to eight actuators. The number of actuators depends on the number of windows and their size. Of the many possible configurations a simple one was selected. The existing building has five 9' by 8' glass partitions on two of the wall encompassing the interior courtyard. Each of these partitions was divided into sixteen 1' high by 4.5' wide windows. Each of these windows would require two actuators.

The sum of the required devices for this setup reaches over 70 amps, which caused an additional 100 amp panel to be added to the electrical configuration. This additional load could not be added to any of the existing panels as it exceeded their spare capacities. It is possible that the additional load could have been spread over the spare capacities of the existing panels. However, for the owners' sake a new panel was added so that the entire system could be controlled from one location if problems occurred. For example if an overload occurred and a fuse switched off, one location could be used, instead of tracking down two to three different panels.

The figure below, Figure 13, is a summary of the electrical load from the new devices.

	Additional Lo	ad Calculation		
Number of Actuators	VA of Actuators	Number of Motor Controllers	VA of Motor Controller	
320	24	40	500	
Number of Outstation Controllers	VA of Outstation Controller	Total VA	Total Amperage	Breaker Size Selected
2	350	28380	70 3ph	100A

Figure 13

Figure 14 is a table displaying the voltage drop calculation. As you can see the voltage drop for the new panel is below 3% and was found to be acceptable.

		Voltage Drop Testing		
Estimated Length	Correction Factor	Calculated Length	Conduit	Voltage
103'	1.1	114'	1.25"	230
VA	Phase	Amps	Power Factor	Wire Size
28080	3	70.4	1	3
Correction Factor	Factor	Voltage Frop	% Drop	Result
1	0.017	1.36	0.59	Acceptable

Figure 14

1.2 Electrical System Reconfiguration

Though the original goal was to was reduce the energy consumption of the new office building enough to reconfigure the electrical system this is not possible. As the results of the hybrid model show, hybrid ventilation was not achievable above 10% in several of the winter months. This means that even though some heating loads may be reduced, the peak heating load remains to be relatively the same, thus the peak electrical load would also remain the same as they occur simultaneously. Because the peak electrical load remains the same the overall system could not be reconfigured.

Construction Breadth Analysis

1.1 Additional Cost Estimates

As previously mentioned the implementation of a hybrid ventilation system would incur additional costs. These not only include the electrical devices for the window automation, but also the pieces for grey water management to feed the water feature, and the wall construction itself.

The total cost of the hybrid ventilation system is estimated to be \$261,479. The most expensive items from the list include the grey water filtration system and the windows. Though it may seem senseless to filter grey water that would only be used for a water feature it is actually a safety precaution to prevent legionellosis. That is why both a standard grey water filter and an Ultra Violet filter were selected. Normally, grey water can be used without this precaution, but the mixing of the water with outdoor air that will be used for natural ventilation was considered and ultimately the filtration systems were selected.

Figures 15through 18 in Appendix A are tables of the mechanical systems cost by item and the percentage of the mechanical costs respectively for the original design and the proposed design.

From the tables you will find that the original cost of the mechanical systems was \$1,309,987. The additional \$261,469 is a 19.9% cost increase. Additionally, you will note that the hybrid ventilation components become the second largest mechanical cost only behind heating and cooling pipes.

1.2 Additional Construction Time

In addition to the additional cost the additional time that would be required to implement the hybrid system was considered. In total it is estimated an additional 827.8 hours would be required. Additionally, the overall schedule was considered. Thankfully, most of the items would not hinder further construction. The window automation devices, software, and electrical systems could be installed by an electrical contractor once the building proceeded to the interiors phase.

The most difficult part of the schedule adjustment would be the excavation required for the cistern and the pipe bedding for the grey water collection and water feature supply. Project documentation and a site visit did indicate that the property was greatly terra-formed to reduce some of the wetlands surrounding the property. It is estimated that the additional earthwork would only add 1 day to the construction time if all of the pieces were in place. For this to happen the cistern and excavator must be on site when the terra-forming is nearing completion. Estimates varied but the conclusion for lead time for the cistern was 1 month. The excavator can be rented from several local offices if the contractor does not already have one. This eases the burden of lead time.

Figure 19 in Appendix A is a table with detailed unit prices and total calculations.

Conclusion

The final results of this report yielded promising results in that the new office building could indeed use hybrid ventilation. An example of this is that it is estimated that 7% of the year the building could use %100 outdoor air. Additionally, the incorporation of a water feature to be used an air cleaner and a source of temperature and humidity regulation proved to be a viable option in conditions at or below 40% outdoor air.

Additionally, the electrical system reconfiguration and adjustment for the load created by the window automation was efficient. The existing system could not accommodate the additional load without dividing it among many panels. Therefore, a 100 Amp panel was added and could be drawn all the back the transformer within acceptable conditions.

Moreover, the additional construction for the hybrid system was found to be minimally invasive on the construction schedule. The only major considerations were towards the cistern, but proper planning and scheduling would make it a non-factor.

However, not all of the goals of this study were achieved. The grey water system was found to be detrimental to the number of hours that hybrid or natural ventilation could be used in outdoor air margins above 40%.

Furthermore, the construction costs of the hybrid system were very much cost prohibitive. At an estimated cost of \$261,479 and an estimated annual savings of \$1,784 the payback period was nowhere near with the acceptable 3 to 5 year range. This is in large part due to the filtration system needed to keep the water and breathable air safe. Additionally, the selected window configuration drove the cost with the number of windows required. Separate configurations were considered, but larger windows were obviously more expensive even of there were less need for the same area. The cost varied minutely.

The final recommendation of this report would be not implement the hybrid ventilation system in the proposed fashion. A much more cost acceptable solution would be to integrate outdoor weather condition sensors with the existing building automation system. A program could be used that emails the occupant under predefined conditions. This would allow for occupants to use operable windows if they so choose.

References

Reese Engineering Inc. "Electrical Construction Documents". State College, PA.

Reese Engineering Inc. "Mechanical Construction Documents". State College, PA.

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NEC: 2011. Quincy, MA: National Fire Protection Association, 2010. Print.

Rsmeans, Engineering Department. Green Building Cost Data 2013. [S.I.]: R S Means, 2012. Print

Mechanical Cost Data 2013. N.p.: R S Means, 2012. Print.

Assemblies Cost Data 2013. N.p.: R S Means, 2012. Print.

Appendix A: General References

Figure 2 depicts the ground level mechanical spaces. This includes the primary space in Area G and the small closet housing an individual heat pump.

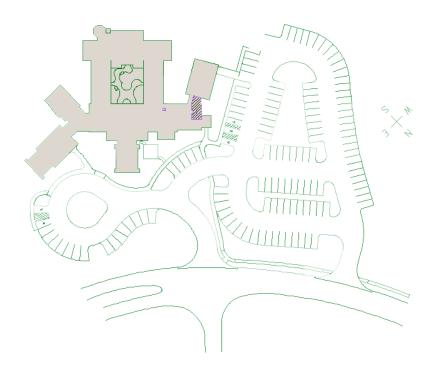


Figure 2

Figure 3 depicts the mezzanine level mechanical spaces. These areas are accessed by a mezzanine storage area in Area H. The ventilation units are isolated above the owners offices in Area E.

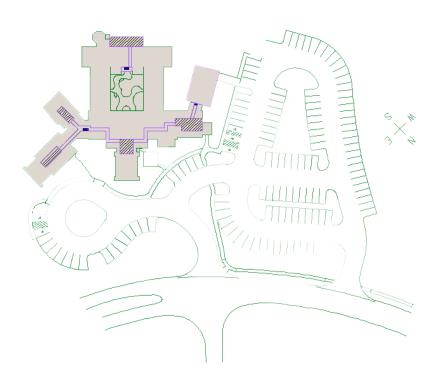


Figure 3

Figure 4 depicts the well field that is under the parking lot. The closed loops exit and enter the building under Area H end then enter the ground level mechanical space.

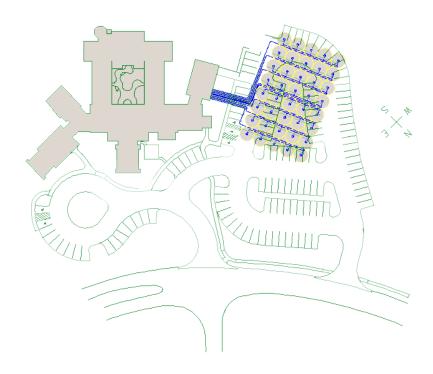


Figure 4

Figure 5 below is an outline of how the geothermal well is utilized. Depicted is the well, the pumps used to move the water to the heat pumps (P-1 and P-2) as well as sensors. The hubs of terminal heat pumps were simplified for this diagram.

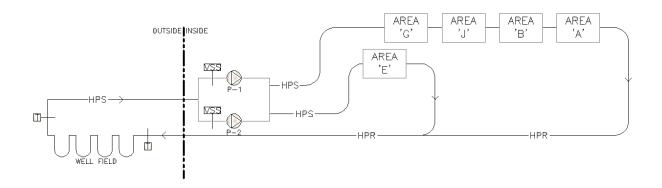


Figure 5

Figure 11 show the number of hours for both standard and water feature conditions that each outdoor air margin can be run. As you will notice the water feature conditions stop being effective after 40% outdoor air.

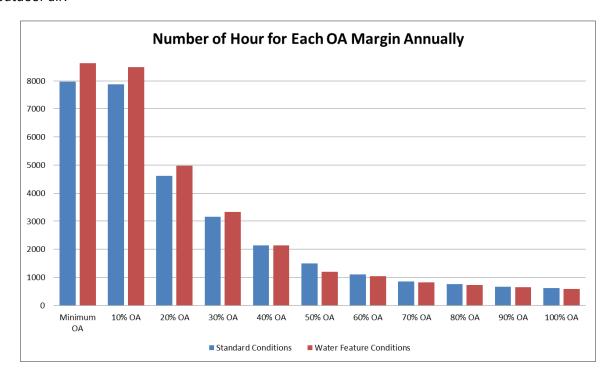


Figure 11

The tables below depict the cost breakdown of mechanical items for the original design and the proposed design. Figure 17 and Figure 18 show the percentage of mechanical costs that each item holds.

Mechanical Item	Cost [\$]	Mechanical Item	Cost [\$]					
Project Coordination	19,800*	Heating & Cooling Piping	280,456					
Temporary Utilities	24,632	Air Handlers	46,037					
Fire Protection	153,400	Heat Pumps	137,862					
Plumbing Piping	99,736	Duct Work	182,241					
Plumbing Specialties	73,642	Fans	24,049					
Plumbing Fixtures	70,213	Air Devices	49,654					
Plumbing Equipment	39,300	Building Controls	128,765					
	Total [\$]	1,309,987						
	Total [\$/SF]] 57.67						

^{*}Project Coordination omitted from total

Figure 15

Mechanical Item	Cost [\$]	Mechanical Item	Cost [\$]
Project Coordination	19,800*	Heating & Cooling Piping	280,456
Temporary Utilities	24,632	Air Handlers	46,037
Fire Protection	153,400	Heat Pumps	137,862
Plumbing Piping	99,736	Duct Work	182,241
Plumbing Specialties	73,642	Fans	24,049
Plumbing Fixtures	70,213	Air Devices	49,654
Plumbing Equipment	39,300	Building Controls	128,765
N/A	N/A	Hybrid Ventilation	261,479
	Total [\$]	1,571,466	
	Total [\$/SF]	69.17	

^{*}Project Coordination omitted from total

Figure 16

Mechanical Item	Percentage of Cost	Mechanical Item	Percentage of Cost [%]
	[%]		
Project Coordination	-	Heating & Cooling Piping	21.4
Temporary Utilities	1.9	Air Handlers	3.5
Fire Protection	11.7	Heat Pumps	10.5
Plumbing Piping	7.6	Duct Work	13.9
Plumbing Specialties	5.6	Fans	1.8
Plumbing Fixtures	5.4	Air Devices	3.8
Plumbing Equipment	3.0	Building Controls	9.8
	Total Cost [\$]	1,309,987	

Figure 17

Mechanical Item	Percentage of Cost	Mechanical Item	Percentage of Cost [%]
	[%]		
Project Coordination	-	Heating & Cooling Piping	17.8
Temporary Utilities	1.6	Air Handlers	2.9
Fire Protection	9.8	Heat Pumps	8.8
Plumbing Piping	6.3	Duct Work	11.6
Plumbing Specialties	4.7	Fans	1.5
Plumbing Fixtures	4.5	Air Devices	3.2
Plumbing Equipment	2.5	Building Controls	8.2
		Hybrid Ventilation	16.6
	Total Cost [\$]	1,309,987	

Figure 18

The table below, Figure 19, is the calculations for the construction cost of the hybrid system. It includes total cost, unit costs, and a summary of the labor required.

	Backfill	Pipe Bedding	Trench Excavation	Soil Removal	Excavation of Soil	Wires	Conductors	Panelboard	Electrical Systems	Pipes	Trench excavation	Grey Water Collection	Pipe	Water Feature	UV Filtration System	Filtration System	Cistern	Water Feature Supply	Control Program	Actuator Package	Window Hardware	Window	CO ₂ Sensor	Humidity Sensor	Temperature Sensor	Motor Controller	Outstation Controller	Window Automation	Item
Total	5	70	70	80	Quantity	1.45	145	1	Quantity	1000	500	Quantity	70	1	1	1	1	Quantity	1	320	160	160	40	40	40	40	2	Quantity	Unit C
Total Hours	C.F.	C.F.	Ľ.F.	C.F.	Units	C.L.F.	L.F.	each	Units	LF.	L.F.	Units	L.F.	each	each	each	each	Units	each	each	each	each	each	each	each	each	each	Units	Unit Details
827.8	0.01	0.025	0.011	0.03		1.6	0.08	2.222		0.101	0.011		0.101	8	8	8	6.4		0	1	1.4	0	0.5	0.5	0.667	0.5	16	Labour Hours	Labor Details
	0	1.69	0	0		124	3.22	147		5.7	0		5.7	550	825	40000	1600		0	219		273	62	385	167	325	945	Material	
	0.43	0.88	0.51	1.28		82.5	4.12	115		4.32	0.51		4.32	284	330	330	400		0	56.5		155	28	28	37	28.5	905	Labor	
Total	1.04	2.57	0.09	1.11		0	0	0		0	0.09		0	0	45	39	0		0	0		0	0	0	0	0	0	Equipment	Cost Details
Total Cost	1.47	5.14	0.6	2.39	Cost per Unit	206.5	7.34	262	Cost per Unit	10.02	0.6	Cost per Unit	10.02	834	1200	40369	2000	Cost per Unit	36	275.5		428	90	413	204	353.5	1850	Cost per Unit	
\$ 261,478.48	7.35	359.8	42	191.2		299.425	1064.3	262		11022	330		701.4	834	1200	40369	2000		36	88160		68480	3600	16520	8160	14140	3700	Total Cost	
					Notes		1.25"	100 A mp	Notes	x1.1 for fittings		Notes		Pump included	For Legionellosis Prevention	Grey water filtration	12,000 Gal Tank. Pump included	Notes			Induded							Notes	Misc.

Figure 20 is a table showing the calculated number of hours each outdoor air margin could be run during the year and what percentage of the year each margin could be achieved. This table is for standard conditions.

Standard	Minimum OA	10% OA	20% OA	30% OA	40% OA	50% OA	60% OA	70% OA	80% OA	90% OA	100% OA
January	31	31	31	31	31	31	31	31	31	31	31
Winter	24	24	0	0	0	0	0	0	0	0	0
Summer	0	0	0	0	0	0	0	0	0	0	0
Febuary	28	28	28	28	28	28	28	28	28	28	28
Winter	24	24	0	0	0	0	0	0	0	0	0
Summer	0	0	0	0	0	0	0	0	0	0	0
March	31	31	31	31	31	31	31	31	31	31	31
Winter	24	24	13	0	0	0	0	0	0	0	0
Summer	0	0	0	0	0	0	0	0	0	0	0
April	30	30	30	30	30	30	30	30	30	30	30
Winter	24	24	24	11	4	0	0	0	0	0	0
Summer	8	8	0	0	0	0	0	0	0	0	0
May	31	31	31	31	31	31	31	31	31	31	31
Winter	11	11	15	17	10	8	6	6	4	6	6
Summer	21	19	13	11	9	9	7	7	7	7	7
June	30	30	30	30	30	30	30	30	30	30	30
Winter	6	7	11	12	8	4	3	3	2	2	2
Summer	24	24	17	14	12	11	9	6	5	3	3
July	31	31	31	31	31	31	31	31	31	31	31
Winter	0	0	6	3	0	0	0	0	0	0	0
Summer	24	24	24	18	13	5	3	0	0	0	0
August	31	31	31	31	31	31	31	31	31	31	31
Winter	7	8	11	13	7	2	1	1	1	0	0
Summer	24	24	16	14	13	10	9	6	5	4	2
September	30	30	30	30	30	30	30	30	30	30	30
Winter	11	11	14	16	10	9	5	4	3	2	2
Summer	23	22	13	10	10	8	7	8	7	7	7
October	31	31	31	31	31	31	31	31	31	31	31
Winter	24	24	24	12	7	4	0	0	0	0	0
Summer	10	9	0	0	0	0	0	0	0	0	0
November	30	30	30	30	30	30	30	30	30	30	30
Winter	24	24	15	7	0	0	0	0	0	0	0
Summer	4	4	0	0	0	0	0	0	0	0	0
December	31	31	31	31	31	31	31	31	31	31	31
Winter	24	24	2	0	0	0	0	0	0	0	0
Summer	0	0	0	0	0	0	0	0	0	0	0
						Total Hours					
Winter	6156	6217	4121	2775	1404	824	457	427	305	306	306
Summer	4219	4096	2543	2053	1745	1314	1069	823	732	641	579
Both	7971	7879	4609	3158	2143	1498	1099	853	762	671	609
			,	,	,	Percentage of Hour		,	,	,	,
Winter	70.3	71.0	47.0	31.7	16.0	9.4	5.2	4.9	3.5	3.5	3.5
Summer	48.2	46.8	29.0	23.4	19.9	15.0	12.2	9.4	8.4	7.3	6.6
Both	91.0	89.9	52.6	36.1	24.5	17.1	12.5	9.7	8.7	7.7	7.0

Figure 20

Figure 21 is a table showing the calculated number of hours each outdoor air margin could be run during the year and what percentage of the year each margin could be achieved. This table is for water feature conditions.

Modified	Minimum OA	10% OA	20% OA	30% OA	40% OA	50% OA	60% OA	70% OA	80% OA	90% OA	100% OA
January	31	31	31	31	31	31	31	31	31	31	31
Winter	24	24	0	0	0	0	0	0	0	0	0
Summer	0	0	0	0	0	0	0	0	0	0	0
Febuary	28	28	28	28	28	28	28	28	28	28	28
Winter	24	24	0	0	0	0	0	0	0	0	0
Summer	0	0	0	0	0	0	0	0	0	0	0
March	31	31	31	31	31	31	31	31	31	31	31
Winter	24	24	13	0	0	0	0	0	0	0	0
Summer	0	0	0	0	0	0	0	0	0	0	0
April	30	30	30	30	30	30	30	30	30	30	30
Winter	24	24	24	11	4	0	0	0	0	0	0
Summer	8	8	0	0	0	0	0	0	0	0	0
May	31	31	31	31	31	31	31	31	31	31	31
Winter	11	11	15	17	10	8	6	6	4	6	6
Summer	21	19	13	11	9	9	7	7	7	7	7
June	30	30	30	30	30	30	30	30	30	30	30
Winter	7	7	12	12	8	4	3	3	2	2	1
Summer	24	24	17	14	12	11	9	6	5	3	3
July	31	31	31	31	31	31	31	31	31	31	31
Winter	0	0	7	3	0	0	0	0	0	0	0
Summer	24	24	24	18	13	5	3	0	0	0	0
August	31	31	31	31	31	31	31	31	31	31	31
Winter	7	8	11	13	6	2	1	1	1	0	0
Summer	24	24	16	14	13	10	9	6	5	4	2
September	30	30	30	30	30	30	30	30	30	30	30
Winter	11	11	14	16	11	8	5	4	3	2	2
Summer	23	20	13	10	10	8	7	8	7	7	7
October	31	31	31	31	31	31	31	31	31	31	31
Winter	24	24	24	12	7	4	0	0	0	0	0
Summer	10	9	0	0	0	0	0	0	0	0	0
November	30	30	30	30	30	30	30	30	30	30	30
Winter	24	24	15	7	0	0	0	0	0	0	0
Summer	4	4	0	0	0	0	0	0	0	0	0
December	31	31	31	31	31	31	31	31	31	31	31
Winter	24	24	1	0	0	0	0	0	0	0	0
Summer	0	0	0	0	0	0	0	0	0	0	0
						Total Hours					
Winter	6186	6217	4151	2775	1403	794	457	427	305	306	276
Summer	4219	4036	2543	2053	1745	1314	1069	823	732	641	579
Both	8637	8485	4983	3331	2143	1190	1038	823	732	641	579
						Percentage of Hour	S				
Winter	70.6	71.0	47.4	31.7	16.0	9.1	5.2	4.9	3.5	3.5	3.2
Summer	48.2	46.1	29.0	23.4	19.9	15.0	12.2	9.4	8.4	7.3	6.6
Both	98.6	96.9	56.9	38.0	24.5	13.6	11.8	9.4	8.4	7.3	6.6

Figure 21

Figure 22 is a table depicting the differences in hours possible for each outdoor air margin for both winter and summer design conditions. Additionally, it shows the difference in percentage that each margin can be run between standard and water feature conditions.

		Differences in Hour Achievable														
Winter	30.0	0.0	30.0	0.0	-1.0	-30.0	0.0	0.0	0.0	0.0	-30.0					
Summer	0.0	-60.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0					
Both	666.0	606.0	374.0	173.0	0.0	-30.0	-30.0									
		666.0 606.0 374.0 173.0 0.0 -308.0 -61.0 -30.0 -30.0 -30.0 -30.0 -30.0 -30.0 Difference in Percenatge of Hours Achievable														
Winter	0.34	0.00	0.34	0.00	-0.01	-0.34	0.00	0.00	0.00	0.00	-0.34					
Summer	0.00	-0.68	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00					
Both	7.60	6.92	4.27	1.97	0.00	-3.52	-0.70	-0.34	-0.34	-0.34	-0.34					

Figure 22

Appendix B: Air Mixing Results for Standard Conditions

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9		7	6	5	4	3	2	1	Hour		
70.5	70.6	70.8	71.0	71.1	71.3	71.4	71.4	71.5	71.5	71.5	71.3	71.1	70.9	70.6	70.3	70.1	70.0	89.9	69.9	70.0	70.1	70.2	70.3	Tmix	Mir	
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	Minimum OA	
0.551	0.550	0.549	0.546	0.544	0.542	0.540	0.537	0.536	0.536	0.538	0.541	0.543	0.547	0.551	0.554	0.556	0.557	0.558	0.558	0.557	0.558	0.554	0.553	RHmix)A	
70.3	70.5	70.6	70.8	71.0	71.1	71.2	71.3	71.4	71.4	71.3	71.2	71.0	70.7	70.4	70.1	69.9	8.69	69.7	69.7	8.69	6.68	70.0	1.07	ximT		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	10% OA	
0.553	0.551	0.550	0.547	0.545	0.543	0.540	0.538	0.537	0.537	0.539	0.542	0.545	0.549	0.553	0.558	0.558	0.559	0.560	0.560	0.559	0.558	0.556	0.554	RHmk		
65.6	85.9	66.3	8.88	66.9	67.2	67.4	67.6	67.7	67.7	67.6	67.4	6.88	66.4	8.29	65.3	64.8	64.6	64.5	64.5	64 66	64.8	65.0	65.3	Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	20% OA	
0.590	0.587	0.584	0.579	0.574	0.570	0.584	0.559	0.557	0.557	0.561	0.567	0.573	0.582	0.590	0.596	0.601	0.603	0.606	0.606	0.604	0.601	0.597	0.594	RHmk		
80.9	61.4	61.9	62.4	62.9	63.3	63.6	63.9	64.1	84.1	64.0	63.5	62.9	62.1	61.2	60.4	59.8	59.3	59.2	59.2	59.4	59.6	0.08	60.4	Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	30% OA	
0.627	0.623	0.618	0.609	0.602	0.595	0.587	0.578	0.575	0.575	0.581	0.591	0.600	0.614	0.628	0.637	0.644	0.647	0.653	0.652	0.648	0.645	0.638	0.633	RHmk		
56.2	56.8	57.5	58.2	58.8	59.4	59.8	60.2	60.4	60.5	60.3	59.7	58.8	57.8	56.6	55.6	54.7	54.7	53.9	54.0	54.2	54.5	55.0	55.6	Tmix		
0.006	0.006	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.008	0.006	0.006	0.006	0.006	0.006	Winix	40% OA	
0.662	0.656	0.651	0.638	0.628	0.619	0.606	0.594	0.590	0.589	0.598	0.613	0.625	0.645	0.664	0.877	0.686	0.690	0.698	0.697	0.691	0.686	0.677	0.670	RHmk		
51.4	52.3	53.1	54.0	54.8	55.5	56.0	58.5	56.8	56.9	56.6	55.9	54.8	53.4	52.0	50.7	49.6	48.9	48.6	48.7	49.0	49.4	50.0	50.7	Trnix		
0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	V/mix	50% OA	January
0.693	0.686	0.680	0.663	0.650	0.638	0.621	0.605	0.600	0.599	0.611	0.630	0.646	0.672	0.696	0.712	0.723	0.727	0.738	0.737	0.729	0.723	0.710	0.702	RHmk		
46.7	47.8	48.8	49.8	50.8	51.6	52.3	52.8	53.1	53.2	52.9	52.1	50.8	49.1	47.4	45.8	44.5	43.7	43.4	43.4	43.8	44.3	45.0	45.8	Tmix		
0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	Wmix	60% OA	
0.716	0.709	0.703	0.682	0.667	0.652	0.631	0.610	0.603	0.603	0.618	0.643	0.661	0.693	0.723	0.741	0.751	0.754	0.770	0.769	0.759	0.751	0.735	0.725	RHmk		
42.0	43.2	44.4	45.6	46.7	47.7	48.5	49.1	49.5	49.6	49.2	48.3	46.7	44.8	42.8	41.0	39.4	38.5	38.1	38.2	38.6	39.2	40.0	41.0	ximT		
0.004	0.004	0.004	0.004	0.005	0.005	0.005	0.004	0.004	0.004	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	V/mix	70% OA	
0.726	0.722	0.718	0.693	0.675	0.659	0.632	0.606	0.598	0.598	0.617	0.648	899.0	0.706	0.739	0.757	0.766	0.765	0.786	0.785	0.772	0.764	0.745	0.736	RHmk		
37.3	38.7	40.0	41.4	42.7	43.8	44.7	45.4	45.8	46.0	45.6	44.4	42.7	40.5	38.2	36.1	34.4	33.2	32.8	32.9	33.4	34.0	35.0	1.96	ximT		
0.003	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	Wmix	80% OA	
0.719	0.719	0.720	0.691	0.672	0.654	0.622	0.590	0.581	0.582	0.605	0.642	0.662	0.705	0.741	0.758	0.758	0.751	0.777	0.777	0.762	0.754	0.734	0.727	RHmk		
32.6	34.1	35.7	37.2	38.6	39.9	40.9	41.7	42.2	42.3	41.9	40.6	38.6	36.2	33.6	31.3	29.3	28.0	27.6	27.7	28.2	28.9	30.0	8.18	ximT		
0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.003	Wmix	90% OA	
0.685	0.694	0.703	0.672	0.654	0.635	0.597	0.559	0.549	0.551	0.578	0.621	0.640	0.685	0.720	0.729	0.727	0.712	0.747	0.747	0.728	0.720	0.695	0.690	RHmk		
27.9	29.6	31.3	33.0	34.6	36.0	37.1	38.0	38.5	38.7	38.2	36.8	34.6	31.9	29.0	26.4	24.2	22.8	22.3	22.4	23.0	23.8	25.0	26.4	Tmix		
0.002	0.002	0.002	0.002	0.003	0.003	0.003	0.002	0.002	0.002	0.003	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	Wmix	100% OA	
0.627	0.645	0.661	0.628	0.613	0.596	0.552	0.508	0.497	0.500	0.533	0.582	0.595	0.640	0.678	0.676	0.651	0.614	0.857	0.658	0.639	0.636	0.616	0.622	RHmk	А	

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	ω	2	1	Hour		
70.5	70.6	70.7	70.9	71.0	71.1	71.2	71.2	71.3	71.3	71.2	71.1	70.9	70.6	70.3	70.1	70.0	69.9	69.9	70.0	70.0	70.1	70.2	70.3	Tmix		
0.009	0.009	0.009	0.009	0.00	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	< Wmix	Minimum OA	
9 0.552	9 0.551	9 0.549	9 0.549	9 0.546	9 0.544	9 0.542	9 0.540	9 0.540	9 0.539	9 0.541	9 0.543	9 0.547	9 0.550	9 0.553	9 0.556	9 0.559	9 0.559	9 0.559	9 0.559	9 0.558	9 0.557	9 0.556	9 0.553	ix RHmix	n OA	
2 70.3	1 70.4	9 70.1	9 70.	6 70.1	4 70.1	2 71.0	0 71.	0 71.	9 71.	1 71.	3 70.1	7 70.	0 70,	3 70.2	9.69	9.69.6	.69	.69	9.69	.69	7 69.9	6 70.1	3 70.2	iix Tmix		
3 0.009	4 0.009	3 0.009	7 0.009	3 0.009	0.009	0.009	1 0.009	1 0.009	1 0.009	1 0.009	0.009	7 0.009	4 0.009	2 0.009	0.009	3 0.009	7 0.009	7 0.009	3 0.009	3 0.009	0.009	0.009	2 0.009	× Wmix	10% OA	
19 0.554	19 0.552	19 0.550	19 0.550	19 0.547	19 0.545	19 0.543	19 0.541	19 0.541	19 0.540	19 0.542	19 0.544	19 0.548	19 0.551	19 0.554	19 0.558	19 0.561	19 0.561	19 0.56	19 0.561	19 0.560	19 0.558	19 0.557	19 0.555	ix RHmix	OA	
4 65.6	65.8	0 66.	.88	17 66.6	66.9	13 67.1	11 67.	11 67.	10 67	12 67.	4 66.9	. 39	65.8	4 65.3	64.8	84.5	22	64.4	64.5	64	64.8	65.0	5 65.3	iix Tmix		
6 0.008	8 0.008	1 0.008	4 0.008	6 0.008	9 0.008	0.008	2 0.008	2 0.008	3 0.008	2 0.008	9 0.008	4 0.008	8 0.008	3 0.008	8 0.008	5 0.008	4 0.008	4 0.008	5 0.008	7 0.008	8 0.008	0.008	3 0.008	x Wmix	20% OA	
8 0.592	8 0.589	8 0.586	8 0.585	8 0.578	8 0.573	8 0.570	8 0.585	8 0.564	8 0.563	8 0.567	8 0.571	8 0.580	8 0.586	8 0.594	0.60	8 0.608	8 0.608	8 0.608	8 0.607	8 0.605	8 0.602	8 0.600	8 0.595	x RHmix)A	
2 60.8	9 61.3	6 61.7	5 62.1	8 62.5	3 62.8	0 63.0	5 63.2	4 63.4	8 63.4	7 63.2	1 62.8	0 62.1	61.3	4 60.5	1 59.8	8 59.3	8 59.1	8 59.2	7 59.3	59.5	2 59.8	0 60.1	5.08	ix Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	< Wmix	30% OA	
7 0.630	0.625	7 0.620	0.619	0.608	0.601	0.595	0.587	0.586	7 0.584	7 0.590	0.597	0.611	0.621	0.632	0.645	7 0.655	0.655	0.657	0.654	0.651	0.646	0.643	0.635	< RHmix)A	
56.1	56.7	57.2	57.8	58.3	58.7	59.0	59.3	59.5	59.6	59.3	58.7	57.8	58.7	55.6	54.7	54.0	53.8	53.9	54.0	54.3	54.7	55.1	55.6	x Tmix		
0.006	0.006	0.006	0.007	0.007	0.007	0.007	0.006	0.007	0.006	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.008	0.006	0.006	0.006	VVmi×	40% OA	
0.667	0.660	0.653	0.652	0.636	0.625	0.618	0.606	0.605	0.601	0.610	0.620	0.639	0.653	0.669	0.687	0.702	0.701	0.704	0.700	0.696	0.689	0.684	0.673	RHmix	Д	
51.4	52.1	52.8	53.4	22	54.6	55.0	55.4	55.6	55.7	55.4	54.6	53.4	52.1	50.8	49.6	48.8	48.6	48.6	48.8	49.1	49.6	50.1	50.8	Tmix		
0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.008	Wmix	50% OA	Febuan
0.700	0.691	0.682	0.682	0.660	0.646	0.636	0.619	0.619	0.614	0.626	0.638	0.664	0.681	0.701	0.725	0.745	0.743	0.747	0.743	0.736	0.727	0.722	0.707	RHmix	•	
46.7	47.5	48.4	49.1	49.9	50.6	51.1	51.5	51.7	51.8	51.5	50.6	49.1	47.5	45.9	44.5	43.6	43.3	43.3	43.6	44.0	44.5	45.1	45.9	Tmix		
0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	Wmix	60% OA	
0.725	0.716	0.706	0.708	0.678	0.661	0.648	0.626	0.626	0.620	0.635	0.649	0.682	0.701	0.725	0.754	0.780	0.777	0.782	0.777	0.769	0.758	0.752	0.733	RHmix		
42.0	42.9	43.9	44.8	45.7	46.5	47.1	47.6	47.8	48.0	47.6	46.5	44.8	42.9	41.1	39.4	38.3	38.0	38.0	38.3	38.8	39.4	40.1	41.1	Tmix		
0.004	0.004	0.004	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	Wmix	70% OA	
0.740	0.731	0.719	0.725	0.688	0.667	0.651	0.623	0.623	0.616	0.635	0.651	0.690	0.710	0.735	0.770	0.801	0.795	0.803	0.797	0.789	0.775	0.770	0.747	RHmix		
37.2	38.4	39.5	40.5	41.6	42.4	43.1	43.6	44.0	44.1	43.6	42.4	40.5	38.4	36.2	34.4	33.1	32.7	32.8	33.1	33.6	34.4	35.2	36.2	Tmix	9	
0.003	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	Wmix	80% OA	
0.737	0.730	0.719	0.731	0.685	0.661	0.642	0.607	0.608	0.599	0.623	0.640	0.684	0.702	0.726	0.764	0.800	0.789	0.801	0.794	0.786	0.771	0.769	0.743	RHmix		
32.5	33.8	35.0	36.2	37.4	38.4	39.1	39.7	40.1	40.3	39.7	38.4	36.2	33.8	31.4	29.3	27.8	27.4	27.5	27.8	28.5	29.3	30.2	31.4	Tmix	9	
0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.003	0.003	Wmix	90% OA	
0.709	0.706	0.699	0.720	0.665	0.637	0.615	0.573	0.576	0.564	0.594	0.610	0.658	0.669	0.689	0.736	0.780	0.764	0.781	0.772	0.763	0.745	0.745	0.712	RHmix		
27.8	29.2	30.6	31.9	33.2	34.3	35.1	35.8	36.2	36.4	35.8	34.3	31.9	29.2	26.5	24.2	22.6	22.1	22.2	22.6	23.3	24.2	25.2	26.5	Tmix :	16	
0.002	0.002	0.002	0.003	0.002	0.002	0.002	0.002	0.002	0.002 1	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002 1	0.002	0.002	0.002	0.002	0.002	0.002	Wmix F	00% OA	
0.658	0.660	0.655	0.686	0.621	0.590	0.566	0.515	0.521	0.507	0.542	0.554	0.603	0.610	0.622	0.663	0.708	0.679	0.704	0.696	0.691	0.676	0.686	0.653	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9		7	6	5	4	S	2	1	Hour		
71.7	71.9	72.1	72.2	72.4	72.5	72.6	72.6	72.5	72.4	72.2	72.0	71.7	71.4	71.1	70.9	70.8	70.8	70.8	70.8	71.0	71.1	71.3	71.5	Tmix		
0.009	0.009	0.009	0.009	0.00	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	< Wmix	Minimum OA	
9 0.542	9 0.540	9 0.538	9 0.536	9 0.533	9 0.530	9 0.528	9 0.527	9 0.527	9 0.528	9 0.530	9 0.533	9 0.537	9 0.541	9 0.545	9 0.548	9 0.551	9 0.551	9 0.550	9 0.550	9 0.548	9 0.547	9 0.545	9 0.544	ix RHmix	n OA	
2 71.5	0 71.	18 71.1	16 72.	13 72.	10 72.	8 72.	72.5	72.	8 72.	10 72.	13 71.8	71.5	11 71.2	.5 71.C	10.1	70.1	70.1	70.1	70.7	10.1	70.1	5 71.	4 71.3	iix Tmix		
5 0.009	7 0.009	0.009	1 0.009	3 0.009	4 0.009	5 0.009	5 0.009	4 0.009	3 0.009	1 0.009	3 0.009	5 0.009	2 0.009	0.009	3 0.009	3 0.009	3 0.009	3 0.009	7 0.009	3 0.009	0.009	1 0.009	3 0.009	× Wmix	10% OA	
19 0.543	19 0.541	19 0.538	19 0.537	19 0.533	19 0.531	19 0.529	19 0.527	19 0.527	19 0.528	19 0.531	19 0.534	19 0.538	19 0.543	19 0.546	19 0.550	19 0.553	19 0.552	19 0.552	19 0.551	19 0.550	19 0.548	19 0.546	19 0.545	ix RHmix	OA	
13 68.1	11 68.5	98 88	89.2	13 69.5	11 69.8	9 69 9	70.0	9.9	9.69	89	88	88	13 67.5	67.0	66.5	33 66.3	2 66.2	2 66.2	1 66.	9.89	99 84	67	67.6	iix Tmix		
0.008	5 0.008	0.008	2 0.008	5 0.008	8 0.008	0.008	0.008	0.008	0.008	2 0.008	7 0.008	0.008	5 0.008	0.008	5 0.008	8 0.008	2 0.008	2 0.008	1 0.008	0.008	0.008	2 0.008	0.008	x Wmix	20% OA	
8 0.571	8 0.566	8 0.561	8 0.557	8 0.551	8 0.545	8 0.54	8 0.538	8 0.537	8 0.540	8 0.545	8 0.551	8 0.560	8 0.569	8 0.577	8 0.584	8 0.591	8 0.590	8 0.589	8 0.588	8 0.585	8 0.582	8 0.578	8 0.575	x RHmix)A	
64.6	85.2	85.8	88.4	8.88	67.2	67.4	87.4	67.3	98.99	66.3	85.5	64.6	83.7	62.9	62.3	61.9	61.8	61.8	82.0	62.4	62.8	63.4	64.0	x Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	0.008	Wmix	30% OA	
0.599	0.592	0.584	0.578	0.568	0.559	0.552	0.547	0.546	0.550	0.557	0.587	0.581	0.595	0.607	0.619	0.630	0.629	0.626	0.625	0.619	0.615	0.609	0.605	RHmix	A	
61.1	62.0	62.8	63.5	64.1	64.6	64.8	64.9	64.7	64.2	63.4	62.3	61.1	0.08	6.83	58.1	57.5	57.4	57.4	57.7	58.2	58.8	59.5	80.3	: Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	40% OA	
0.626	0.616	0.606	0.598	0.583	0.571	0.562	0.554	0.552	0.558	0.567	0.580	0.599	0.618	0.635	0.652	0.668	0.666	0.663	0.661	0.654	0.648	0.639	0.634	RHmix		
57.8	58.7	59.7	8.08	61.4	62.0	62.3	62.4	62.1	61.5	60.5	59.1	57.6	56.2	54.9	53.9	53.1	52.9	53.1	53.4	54.0	54.7	55.6	8.85	Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.008	Wmix	50% OA	March
0.653	0.640	0.627	0.617	0.598	0.581	0.570	0.558	0.556	0.563	0.574	0.591	0.614	0.639	0.661	0.683	0.705	0.702	0.697	0.695	0.685	0.679	0.668	0.662	RHmix		
54.2	55.4	56.6	57.7	58.6	59.3	59.8	59.9	59.6	58.8	57.5	56.0	54.2	52.4	50.9	49.6	48.8	48.5	48.7	49.1	49.7	50.6	51.7	52.9	Tmix		
0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.006	0.006	Wmix	60% OA	
0.678	0.662	0.646	0.634	0.610	0.590	0.575	0.580	0.557	0.564	0.577	0.597	0.625	0.656	0.682	0.710	0.739	0.734	0.727	0.726	0.713	0.707	0.693	0.688	RHmix		
50.7	52.2	53.6	54.8	55.9	56.7	57.2	57.4	57.0	56.1	54.6	52.8	50.7	48.7	46.9	45.4	44.4	44.1	44.3	44.8	45.5	46.6	47.8	49.2	Tmix	7	
0.005	0.006	0.006	0.008	0.006	0.006	0.006	0.008	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	VVmix	70% OA	
0.699	0.682	0.663	0.650	0.620	0.595	0.577	0.558	0.554	0.561	0.576	0.598	0.630	0.886	969.0	0.731	0.767	0.759	0.750	0.750	0.735	0.729	0.714	0.710	RHmix		
47.2	48.9	50.5	52.0	53.2	54.1	54.7	54.8	54.4	53.4	51.7	49.6	47.2	44.9	42.8	41.2	40.0	39.7	39.9	40.4	41.3	42.5	44.0	45.6	Tmix	9	
0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.005	Wmix	80% OA	
0.717	0.698	0.677	0.662	0.627	0.597	0.575	0.552	0.546	0.554	0.568	0.591	0.627	0.667	0.701	0.741	0.785	0.774	0.762	0.764	0.747	0.743	0.727	0.726	RHmix		
43.8	45.7	47.5	49.1	50.4	51.5	52.1	52.3	51.9	50.7	48.8	46.5	43.8	41.2	38.8	36.9	35.7	35.3	35.5	36.1	37.1	38.5	40.1	41.9	Tmix	9	
0.004	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.004	0.004	0.004	Wmix F	90% OA	
0.728	0.708	0.686	0.671	0.629	0.595	0.569	0.541	0.533	0.539	0.553	0.576	0.613	0.656	0.691	0.736	0.789	0.773	0.758	0.763	0.746	0.746	0.731	0.735	RHmix		
40.3 (42.4 (44.4	46.2 (47.7 (48.9 (49.6 (49.8 (49.3 (48.0 (45.9	43.3 (40.3	37.4 (34.8 (32.7 (31.3	30.9 (31.1	31.8 0	32.9	34.4 (36.2	38.2 (Tmix \	10	
0.004 (0.004 0	0.004 0	0.004 (0.004 0	0.004 0	0.004 0	0.004 0	0.004 (0.004 0	0.003 (0.003 0	0.003 0	0.003 (0.003 0	0.003 (0.003 0	0.003 (0.003 (0.003 0	0.003 (0.003 0	0.003 0	0.004 (Wmix F	00% OA	
0.731	0.712	0.690	0.875	0.627	0.587	0.557	0.524	0.513	0.518	0.529	0.550	0.586	0.629	0.663	0.711	0.776	0.753	0.734	0.741	0.724	0.732	0.720	0.733	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	Hour		
72.6	72.8	73.0	73.1	73.2	73.4	73.4	73.4	73.4	73.3	73.1	72.8	72.6	72.3	72.1	71.9	71.8	71.7	71.7	71.8	71.9	72.0	72.2	72.4	Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	< Wmix	Minimum OA	
9 0.536	9 0.534	9 0.532	9 0.530	9 0.527	9 0.525	9 0.524	9 0.523	9 0.523	9 0.523	9 0.524	9 0.526	9 0.529	9 0.532	9 0.535	9 0.538	9 0.542	9 0.543	9 0.542	9 0.543	9 0.542	9 0.540	9 0.538	9 0.537	ix RHmix	n OA	
6 72.5	4 72.	2 72.9	0 73.0	7 73.2	5 73.3	4 73.	3 73.4	9 79.3	3 73.3	4 73.0	6 72.8	9 72.5	2 72.3	5 72.0	8 71.8	2 71.6	3 71.6	2 71.6	3 71.7	2 71.8	0 71.9	8 72.	7 72.3	iix Tmix		
5 0.009	7 0.009	0.009	0.009	2 0.009	0.009	1 0.009	1 0.009	0.009	2 0.009	0.009	0.009	0.009	2 0.009	0.009	0.009	0.009	0.009	0.009	7 0.009	0.009	0.009	0.009	8 0.009	× Wmix	10% OA	
9 0.536	9 0.534	9 0.533	9 0.530	9 0.528	9 0.526	9 0.524	9 0.523	9 0.523	9 0.523	9 0.524	9 0.527	9 0.530	9 0.532	9 0.535	9 0.539	9 0.543	9 0.544	9 0.543	9 0.544	9 0.543	9 0.541	9 0.539	9 0.538	ix RHmix)A	
3 70.0	70.4	3 70.7	71.1	8 71.4	6 71.6	4 71.7	3 71.8	3 71.7	3 71.4	71.0	70.5	0.07	2 69.4	68.9	68.5	8 88 3	4 68.2	3 68.2	68.4	3 68.6	1 68.9	89.2	9.69	ix Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.009	0.009	0.009	: Wmix	20% OA	
0.558	0.553	0.551	0.545	0.540	0.536	0.532	0.530	0.531	0.531	0.532	0.537	0.544	0.548	0.555	0.563	0.572	0.573	0.571	0.572	0.572	0.568	0.564	0.561	RHmix	A	
67.4	0.88	68.6	69.1	69.5	69.9	70.1	70.1	70.0	69.6	69.0	68.3	67.4	8.88	65.9	65.3	64.9	64.8	64.8	65.0	65.3	65.8	66.3	8.33	Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	30% OA	
0.579	0.572	0.568	0.560	0.552	0.545	0.539	0.536	0.537	0.537	0.539	0.546	0.556	0.563	0.573	0.586	0.600	0.602	0.600	0.602	0.601	0.594	0.588	0.585	RHmix	,	
64.9	65.7	66.5	67.2	67.7	68.2	68.4	68.5	68.3	67.8	67.0	0.88	64.9	63.8	62.8	62.0	61.5	61.4	61.4	61.7	62.1	62.7	63.4	64.1	Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	0.008	0.008	Wmix	40% OA	
0.601	0.591	0.586	0.575	0.564	0.554	0.546	0.542	0.543	0.542	0.545	0.554	0.568	0.577	0.590	0.608	0.629	0.631	0.628	0.631	0.631	0.621	0.613	0.608	RHmix		
62.4	63.4	64.4	65.2	65.9	66.5	8.33	66.9	66.6	0.88	65.0	63.8	62.4	61.0	8.85	58.8	58.1	58.0	58.0	58.4	9.85	59.6	60.5	61.4	Tmix		
0.007	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	50% OA	April
0.623	0.610	0.604	0.589	0.575	0.563	0.552	0.547	0.548	0.547	0.550	0.560	0.577	0.589	0.605	0.628	0.657	0.660	0.655	0.660	0.661	0.648	0.637	0.632	RHmix		
59.9	61.1	62.2	63.2	64.1	64.7	65.2	65.3	65.0	64.3	63.1	61.6	59.9	58.3	56.8	55.6	54.8	54.5	54.7	55.1	55.7	56.6	57.6	58.7	Tmix	3	
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.007	0.007	0.007	Wmix	60% OA	
0.644	0.629	0.622	0.604	0.586	0.571	0.558	0.551	0.552	0.550	0.552	0.584	0.585	0.598	0.617	0.646	0.684	0.687	0.682	0.689	0.690	0.674	0.661	0.655	RHmix		
57.4	58.8	60.1	61.3	62.3	63.0	63.5	63.7	63.3	62.5	61.1	59.3	57.4	55.5	53.7	52.3	51.4	51.1	51.3	51.8	52.5	53.5	54.7	56.0	Tmix	7	
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	0.006	0.006	0.008	0.005	0.005	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.008	Wmix I	70% OA	
0.665	0.647	0.640	0.618	0.597	0.578	0.562	0.554	0.556	0.552	0.554	0.566	0.590	0.603	0.626	0.661	0.709	0.713	0.706	0.716	0.718	0.699	0.684	0.678	RHmix		
54.8	56.4	58.0	59.3	60.4	61.3	61.9	62.0	61.6	60.7	59.1	57.1	54.8	52.7	50.7	49.1	48.0	47.7	47.9	48.4	49.2	50.4	51.8	53.2	Tmix	8	
0.006	0.006	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.006	0.006	0.008	Wmix F	80% OA	
0.686	0.665	0.657	0.631	0.606	0.584	0.566	0.558	0.558	0.553	0.553	0.565	0.592	0.605	0.630	0.671	0.731	0.735	0.726	0.740	0.745	0.723	0.705	0.699	RHmix		
52.3	54.1	55.8	57.4	58.6	59.6	80.2	60.4	60.0	58.9	57.1	54.8	52.3	49.9	47.6	45.8	44.7	44.3	44.5	45.1	46.0	47.4	48.9	50.5	Tmix 1	91	
0.006 (0.006 (0.006 (0.006 (0.006 (0.006 (0.006 (0.006 (0.006 (0.006 (0.005 (0.005 (0.005 (0.005 (0.004 (0.004 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.006 (Wmix F	90% OA	
0.705	0.682	0.674	0.644	0.615	0.590	0.568	0.557	0.558	0.551	0.549	0.562	0.590	0.602	0.627	0.675	0.748	0.753	0.742	0.761	0.769	0.743	0.724	0.720	RHmix		
49.8 (51.8 0	53.7 0	55.4 0	56.8 0	57.9 0	58.6	58.8 0	58.3 (57.1 0	55.1 0	52.6 0	49.8 0	47.1 0	44.6	42.6 (41.3 0	40.9 (41.1 0	41.8 0	42.8 (44.3 (46.0 0	47.8 (Tmix \	10	
0.005 0	0.006 0	0.006 0	0.008 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.005 0	0.005 0	0.005 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.005 0	0.005 0	0.005 0	0.005 0	Wmix R	00% OA	
0.723	0.698	0.691	0.656	0.623	0.594	0.569	0.556	0.557	0.548	0.543	0.554	0.583	0.592	0.617	0.672	0.760	0.764	0.751	0.777	0.789	0.761	0.740	0.738	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	80	7	6	5	4	ω	2	1	Hour		
73.8	74.1	74.4	74.6	74.9	75.1	75.2	75.2	75.2	75.1	74.9	74.6	74.4	74.1	73.8	73.5	73.2	73.1	72.9	72.9	72.9	73.1	73.2	73.5	Tmix		
0.009	0.009	0.009	0.009	0.00	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	< Wmix	Minimum OA	
9 0.521	9 0.520	9 0.518	9 0.515	9 0.511	9 0.508	9 0.506	9 0.505	9 0.506	9 0.507	9 0.508	9 0.510	9 0.513	9 0.517	9 0.520	9 0.524	9 0.529	9 0.532	9 0.533	9 0.533	9 0.532	9 0.530	9 0.527	9 0.525	ix RHmix	n OA	
1 73.7	0 74.0	8 74.3	5 74.8	1 74.9	8 75.	6 75.3	5 75.3	6 75.3	7 75.	8 74.9	0 74.6	3 74.3	7 74.0	0 73.3	4 73,4	9 73.3	2 73.0	3 72.9	3 72.8	2 72.8	0 73.0	7 73.3	5 73.4	iix Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	< Wmix	10% OA	
9 0.522	9 0.520	9 0.518	9 0.515	9 0.511	9 0.507	9 0.506	9 0.505	9 0.505	9 0.507	9 0.508	9 0.510	9 0.512	9 0.517	9 0.520	9 0.524	9 0.529	9 0.533	9 0.534	9 0.534	9 0.532	9 0.530	9 0.528	9 0.525	ix RHmix)A	
2 72.4	73.1	8 73.7	5 74.3	1 74.8	7 75.1	8 75.4	5 75.5	5 75.4	75.1	8 74.8	0 74.3	2 73.7	7 73.1	0 72.4	4 71.8	71.3	3 71.0	4 70.7	70.6	2 70.7	71.0	8 71.3	5 71.8	ix Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	< Wmix	20% OA	
0.527	0.524	0.520	0.514	0.505	0.499	0.496	0.494	0.495	0.498	0.500	0.504	0.509	0.517	0.524	0.532	0.543	0.550	0.552	0.552	0.549	0.545	0.540	0.535	< RHmix)A	
71.2	72.1	73.0	73.9	74.6	75.2	75.6	75.7	75.6	75.2	74.6	73.9	73.0	72.1	71.2	70.3	69.5	68.9	68.6	68.5	68.6	68.9	69.5	70.3	< Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.009	Wmix	30% OA	
0.532	0.529	0.522	0.513	0.500	0.491	0.486	0.483	0.485	0.489	0.493	0.499	0.505	0.517	0.527	0.540	0.556	0.587	0.571	0.571	0.567	0.560	0.552	0.544	RHmix	14	
69.9	71.1	72.4	73.5	74.5	75.3	75.8	75.9	75.8	75.3	74.5	73.5	72.4	71.1	69.9	68.7	67.7	66.9	66.4	66.3	66.4	66.9	67.7	68.7	Tmix		
0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	VVmi×	40% OA	
0.537	0.532	0.523	0.512	0.495	0.483	0.476	0.473	0.474	0.480	0.485	0.492	0.501	0.517	0.530	0.548	0.569	0.585	0.589	0.589	0.584	0.575	0.564	0.553	RHmix		
68.6	70.2	71.7	73.2	74.4	75.3	76.0	76.2	76.0	75.3	74.4	73.2	71.7	70.2	68.6	67.1	65.9	64.9	64.3	92.1	64.3	64.9	65.9	1.78	Tmix		
0.008	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	50% OA	May
0.542	0.536	0.525	0.510	0.489	0.475	0.486	0.462	0.464	0.471	0.477	0.486	0.496	0.516	0.533	0.555	0.582	0.603	0.608	0.608	0.601	0.589	0.575	0.582	RHmix		
67.3	69.2	71.0	72.8	74.3	75.4	76.1	76.4	76.1	75.4	74.3	72.8	71.0	69.2	67.3	65.5	64.0	62.9	62.2	61.9	62.2	62.9	64.0	65.5	Tmix	9	
0.008	0.008	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.007	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.008	Wmix	60% OA	
0.546	0.540	0.526	0.509	0.484	0.466	0.457	0.452	0.455	0.462	0.469	0.479	0.491	0.515	0.534	0.561	0.595	0.621	0.627	0.627	0.617	0.603	0.586	0.570	RHmix		
66.0	68.2	70.4	72.4	74.2	75.5	76.3	76.6	76.3	75.5	74.2	72.4	70.4	68.2	0.88	63.9	62.2	80.9	60.0	59.7	0.08	60.9	62.2	63.9	Tmix	7	
0.007	0.008	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix I	70% OA	
0.549	0.543	0.527	0.508	0.479	0.458	0.447	0.442	0.445	0.454	0.461	0.473	0.486	0.513	0.535	0.567	0.608	0.639	0.646	0.646	0.634	0.617	0.596	0.578	RHmix		
64.8	67.2	69.7	72.0	74.0	75.6	76.5	76.8	76.5	75.6	74.0	72.0	69.7	67.2	64.8	62.4	60.4	58.8	57.9	57.6	57.9	58.8	60.4	62.4	Tmix 1	81	
0.007	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix F	80% OA	
0.552	0.546	0.529	0.506	0.473	0.450	0.438	0.432	0.435	0.445	0.453	0.486	0.480	0.511	0.536	0.571	0.620	0.657	0.665	0.664	0.650	0.630	0.606	0.585	RHmix		
63.5	66.3	69.1	71.7	73.9	75.6	76.7	77.1	76.7	75.6	73.9	71.7	69.1	88.3	63.5	8.08	58.5	56.8	55.7	55.4	55.7	56.8	58.5	8.08	Tmix 1	90	
0.007 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.007 (0.007 (0.007 (0.006 (0.007 (0.007 (0.006 (0.006 (0.006 (0.006 (0.006 (0.007 (Wmix F	90% OA	
0.555	0.548	0.530	0.504	0.467	0.442	0.429	0.422	0.425	0.436	0.445	0.459	0.474	0.508	0.535	0.575	0.631	0.674	0.683	0.682	0.665	0.641	0.614	0.592	RHmix		
62.2 0	65.3 0	68.4 0	71.3 0	73.8 0	75.7 0	76.9 0	77.3 0	76.9 0	75.7 0	73.8 0	71.3 0	68.4 0	65.3 0	62.2 0	59.2 0	56.7 0	54.8 0	53.6 0	53.2 0	53.6 0	54.8 0	56.7 0	59.2 0	Tmix V	100	
0.007 0	0.007 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.007 0	0.007 0	0.007 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	Wmix R	00% OA	
0.556	0.551	0.530	0.503	0.462	0.434	0.419	0.412	0.416	0.428	0.437	0.451	0.467	0.505	0.533	0.578	0.642	0.692	0.701	0.699	0.679	0.652	0.622	0.597	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	Hour		
74.5	74.8	75.0	75.2	75.4	75.5	75.6	75.6	75.6	75.4	75.3	75.0	74.8	74.5	74.2	74.0	73.8	73.7	73.7	73.7	73.8	73.9	74.1	74.3	Tmix		
5 0.010	8 0.010	0.010	2 0.010	4 0.010	5 0.010	3 0.010	3 0.010	3 0.010	4 0.010	3 0.010	0.010	8 0.010	5 0.010	2 0.009	0.009	3 0.009	7 0.010	7 0.010	7 0.010	3 0.009	0.010	0.010	3 0.010	× Wmix	Minimum OA	
0 0.534	0 0.533	0 0.531	0 0.529	0 0.522	0 0.517	0 0.51	0 0.51	0 0.514	0 0.517	0.5	0 0.519	0 0.521	0 0.523	19 0.526	0.530	19 0.534	0 0.538	0 0.538	0 0.538	0.535	0 0.534	0 0.534	0 0.535	ix RHmix	m OA	
74	13 74.	31 75.	75.	22 75.	75.	5 75.	4 75.	4 75.	75.	18 75.	9 75.	74.	23 74.5	26 74.	74.0	73.	38 73.7	38 73.	38 73.7	35 73.	73.	34 74.1	35 74.3	nix Tmix		
.5 0.010	7 0.010	0.010	2 0.010	4 0.010	5 0.010	6 0.010	6 0.010	6 0.010	5 0.010	3 0.010	0.010	8 0.010	5 0.010	2 0.009	0.009	8 0.009	7 0.010	6 0.010	7 0.010	7 0.009	9 0.010	1 0.010	3 0.010	× Wmix	10% OA	
10 0.535	10 0.533	10 0.532	10 0.529	10 0.522	10 0.517	10 0.515	10 0.514	10 0.514	10 0.517	10 0.518	10 0.520	10 0.521	10 0.523	19 0.526	0.531	19 0.535	10 0.539	10 0.539	10 0.538	19 0.536	10 0.534	10 0.535	10 0.538	ıix RHmix	OA	
74	74	32 75.0	29 75.4	22 75.7	17 76	15 76.2	14 76.2	14 76	75	18 75	20 75.	74	23 74.0	26 73.4	31 72.9	35 72.6	39 72.3	39 72.3	38 72.3	36 72.5	34 72	35 73	36 73.5	nix Tmix		
.0 0.010	.5 0.010	0 0.01	4 0.010	7 0.010	0 0.010	2 0.010	2 0.010	2 0.010	.9 0.010	6 0.010	.1 0.010	.5 0.010	0.009	4 0.009	9 0.009	6 0.009	3 0.010	3 0.009	3 0.009	5 0.009	8 0.009	.1 0.010	5 0.010	ix Wmix	20% OA	
10 0.555	10 0.55	10 0.548	10 0.542	10 0.528	10 0.5	10 0.515	10 0.512	10 0.512	10 0.51	10 0.519	10 0.523	10 0.527	0.531	0.537	0.547	0.555	10 0.563	0.563	0.562	0.557	0.554	10 0.555	10 0.558	nix RHmix	OA	
55 73.5	51 74.2	48 74.9	42 75.6	28 76.	18 76.5	15 76.8	12 76.9	12 76.	18 76.4	19 75.8	23 75.	27 74.3	31 73.4	37 72.6	47 71.9	55 71.3	63 71	63 70.9	62 71.0	57 71.2	54 71	55 72.2	58 72.8	nix Tmix		
.5 0.010	.2 0.010	.9 0.010	.6 0.010	.1 0.010	.5 0.010	8 0.010	9 0.010	.7 0.010	4 0.010	.8 0.010	.1 0.010	.3 0.010	.4 0.009	.6 0.009	9 0.009	.3 0.009	.0 0.010		0		.6 0.009	.2 0.010	.8 0.010	ix Wmix	30% OA	
10 0.575	10 0.570	10 0.564	10 0.555	10 0.534	-		10 0.510		0	10 0.521	10 0.527		0.539	09 0.549	0	0.575	10 0.589	.009 0.5	.009 0.5	.009 0.5	09 0.574	10 0.575	10 0.580	nix RHmix	OA	
75 73.	70 74	64 74	55 75	34 76	.519 77.0	.514 77.4	10 77.5	.509 77.3	.519 76	21 76.1	27 75.2	.532 74.1	39 72.9	49 71.8	.563 70.9	75 70.1	89 69	.589 69	.587 69	.579 70.0	74 70	75 71.2	80 72.1	nix Tmix		
.0 0.010	.0 0.01	.9 0.01	.8 0.01	.5 0.01	.0 0.010	.4 0.010	.5 0.010	.3 0.010	.8 0.010	.1 0.010	.2 0.010	.1 0.010	.9 0.009	.8 0.009	0	.1 0.009	.7 0.010	.5 0	.6 0.009	.0 0.009	.5 0		.1 0.010	iix Winix	40% OA	
10 0.596	11 0.588	11 0.581	11 0.568	11 0.540	10 0.520	10 0.513	10 0.509	10 0.507	10 0.520	10 0.523	10 0.531	10 0.538	09 0.547	09 0.560	.009 0.580	09 0.597	10 0.616	.009 0.615	09 0.614	09 0.603	.009 0.596	.010 0.597	10 0.602	nix RHmix	OA	
96 72.5	88 73.7	81 74	68 76.0	40 76	20 77	13 78	09 78.1	07 77.9	20 77.3	23 76.4	31 75.2	38 73.8	47 72.4	60 71.0	80 69	88	68	15 68.1	14 68	03 68.7	96 69	97 70.3	02 71.3	nix Tmix		
.5 0.011	.7 0.01	.9 0.01	.0 0.01	.8 0.01	.5 0.010	.0 0.010	.1 0.010	.9 0.010	.3 0.010	.4 0.010	.2 0.010	.8 0.010	.4 0.009	.0 0.009	.8 0.009	.9 0.009	.4 0.009	.1 0.009	.3 0.009	.7 0.009	.4 0.009	.3 0.010	.3 0.010	ix Wmix	50% OA	June
11 0.618	11 0.607	11 0.597	11 0.58	11 0.548	10 0.520	10 0.512	10 0.507	10 0.505	10 0.520	10 0.525	10 0.535	10 0.543	0.556	09 0.572	0.598	0.620	0.644	0.644	09 0.642	09 0.627	9.0 60	0.6	10 0.626	nix RHmix	OA	ne en
18 72.0	07 73.4	37 74.9	31 76.	46 77.2	20 78.	12 78.5	J7 78.	35 78.5	20 77.8	25 76.	35 75.2	13 73.6	56 71.9	72 70.3	98 88 86	20 67.7	44 67.0	14 66.8	12 66.9	27 67.4	18 68.3	19 69.4	26 70.6	nix Tmix		
0 0.011	4 0.01	9 0.01	1 0.01	2 0.01	1 0.01	5 0.01	7 0.01	5 0.010	8 0.01	7 0.010	2 0.010	6 0.010	9 0.009	3 0.009	8 0.009	7 0.009	0 0.009	8 0.009	9 0.009	4 0.009	3 0.009	4 0.010	6 0.010	ix Wmix	60% OA	
1 0.640	1 0.626	1 0.613	1 0.593	1 0.55	1 0.521	1 0.51	1 0.504	0 0.502	1 0.521	0 0.526	0 0.539	0 0.549	0.584	0.584	0.616	0.643	19 0.674	19 0.673	19 0.671	19 0.652	9 0.64	0 0.643	0.650	ix RHmix	OA	
10 71.5	26 73.2	3 74.	33 76.	51 77.6	78.	1 79.	14 79.	12 79.	78.	26 77.0	39 75.	19 73.	71.4	84 69.	67.	13 66.	4 65.	73 65.4	11 65.	52 66.	H 67.2	13 68.4	69	nix Tmix		
5 0.011	2 0.011	9 0.012	3 0.01	6 0.011	6 0.011	1 0.011	3 0.011	1 0.011	2 0.011	0.010	3 0.010	4 0.010	4 0.009	5 0.00	8 0.009	5 0.009	7 0.009	0.0	6 0.009	2 0.00	0.0	0.01	.9 0.011	× Wmix	70%	
1 0.862	1 0.645	2 0.629	12 0.605	1 0.557	1 0.521	1 0.510	1 0.502	1 0.500	1 0.521	0 0.528	0 0.543	0 0.555	19 0.572	19 0.596	19 0.635	19 0.668	19 0.705	0.705	19 0.701	19 0.679	0.665	0.667	1 0.676	ix RHmix	OA	
12 71.0	15 72.9	9 74.8	76.5	78.0	79.1	0 79.7	12 80.0	0 79.6	78.7	8 77.2	75.3	5 73.2	70.8	16 68.7	8.89	8 65.2	15 64.4	64.0	11 64.2	9 64.9	66.0	67.5	6 69.2	nix Tmix		
0 0.011	9 0.011	8 0.012	5 0.012	0 0.011	1 0.011	7 0.011	0 0.011	6 0.011	7 0.011	2 0.011	3 0.010	2 0.010	8 0.009	7 0.009	8 0.009	2 0.009	4 0.009	0 0.009	2 0.009	9 0.009	0 0.009	5 0.010	2 0.011	ix Wmix	80% OA	
1 0.686	1 0.665	2 0.646	2 0.618	1 0.562	1 0.521	1 0.509	1 0.500	1 0.498	1 0.522	1 0.529	0 0.546	0.560	9 0.581	9 0.609	9 0.654	9 0.694	9 0.738	9 0.738	9 0.734	9 0.707	9 0.690	0 0.692	1 0.702	ix RHmix	OA	
6 70.5	5 72.7	6 74.8	8 76.7	2 78.3	79.6	80.3	9.08	18 80.2	2 79.1	9 77.5	6 75.4	0 72.9	70.3	9 67.9	4 65.7	64.0	8 63.0	18 62.7	62.9	7 63.7	0 64.9	2 66.5	2 68.4	iix Tmix		
0.011	7 0.012	8 0.012	7 0.012	0.012	0.011	8 0.011	0.011	2 0.011	0.011	5 0.011	0.010	0.010	0.009	0.009	7 0.009	0.009	0.009	7 0.009	0.009	7 0.009	0.009	0.010	1 0.011	x Wmix	90% OA	
1 0.709	2 0.685	2 0.662	2 0.630	2 0.567	1 0.522	1 0.507	1 0.498	1 0.495	1 0.522	1 0.531	0 0.550	0 0.566	9 0.590	9 0.622	9 0.674	9 0.721	9 0.773	9 0.772	9 0.768	9 0.736	9 0.716	0 0.718	1 0.729	ix RHmix)A	
9 70.0	5 72.4	2 74.8	0 76.9	7 78.7	2 80.1	7 80.9	8 81.2	8.08	2 79.6	1 77.8	0 75.4	6 72.7	8.89	2 67.1	4 64.7	1 62.8	3 61.7	2 61.3	8 61.5	6 62.4	6 63.8	9.59	9 67.7	iix Tmix		
0.011	0.012	0.013	0.013	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.010	0.011	< Wmix	100% OA	
1 0.734	2 0.705	3 0.678	3 0.641	2 0.571	1 0.522	1 0.506	1 0.495	1 0.492	1 0.522	1 0.532	0 0.554	0 0.572	19 0.599	19 0.635	19 0.695	19 0.749	9 0.809	19 0.809	19 0.804	19 0.767	19 0.743	0 0.745	1 0.757	ix RHmix	OA	
Ä	9	8	7	1	12	ത്	5	72	ž	32	7	2	99	ŭ	55	õ	9	9	Z	37	ದ	σ'n	57	×		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	з	2	1	Hour		
74.7	74.9	75.1	75.3	75.5	75.6	75.8	75.9	75.9	75.9	75.9	75.8	75.6	75.3	75.1	74.8	74.6	74.4	74.2	74.2	74.2	74.3	74.4	74.5	Tmix	M	
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	Wmix	Minimum (
0.537	0.537	0.534	0.533	0.529	0.524	0.520	0.520	0.520	0.522	0.525	0.527	0.530	0.532	0.536	0.538	0.543	0.546	0.544	0.542	0.542	0.540	0.539	0.538	RHmix	OA	
74.7	74.9	75.1	75.3	75.5	75.6	75.8	75.9	76.0	76.0	75.9	75.8	75.6	75.4	75.1	74.8	74.5	74.3	74.2	74.2	74.2	74.3	74.4	74.5	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	Wmix	10% OA	
0.538	0.538	0.535	0.534	0.530	0.525	0.520	0.520	0.520	0.522	0.525	0.528	0.530	0.533	0.536	0.539	0.544	0.547	0.545	0.543	0.543	0.541	0.540	0.539	RHmix		
74.4	74.7	75.2	75.6	75.9	76.3	76.6	76.8	76.9	77.0	76.9	76.6	76.2	75.7	75.2	74.6	74.1	73.7	73.4	73.3	73.4	73.5	73.7	74.0	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	Wmix	20% OA	
0.580	0.560	0.554	0.552	0.544	0.533	0.523	0.523	0.524	0.528	0.533	0.539	0.544	0.550	0.557	0.563	0.574	0.580	0.576	0.572	0.571	0.567	0.566	0.562	RHmix		
74.0	74.6	75.2	75.8	76.4	76.9	77.3	77.7	77.9	77.9	77.8	77.4	76.8	76.1	75.2	74.4	73.6	73.0	72.6	72.5	72.6	72.8	73.1	73.5	Tmix		
0.010	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	Wmix	30% OA	
0.583	0.582	0.573	0.569	0.557	0.541	0.527	0.526	0.527	0.534	0.541	0.549	0.557	0.587	0.577	0.586	0.604	0.614	0.608	0.603	0.600	0.595	0.592	0.586	RHmix		
73.7	74.5	75.3	76.1	76.9	77.6	78.1	78.6	78.8	78.9	78.8	78.2	77.4	76.4	75.3	74.2	73.2	72.4	71.8	71.7	71.8	72.0	72.5	73.0	Tmix		
0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.011	0.011	VVmix	40% OA	
0.606	0.605	0.591	0.587	0.569	0.549	0.529	0.529	0.530	0.538	0.547	0.558	0.570	0.583	0.598	0.610	0.635	0.649	0.642	0.634	0.631	0.623	0.619	0.611	RHmix		
73.4	74.3	75.4	76.4	77.3	78.2	78.9	79.5	79.8	79.9	79.7	79.0	78.0	76.8	75.4	74.0	72.7	71.7	71.0	70.8	71.0	71.3	71.8	72.5	Tmix		
0.011	0.011	0.011	0.012	0.012	0.011	0.011	0.011	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	Wmix	50% OA	July
0.629	0.627	0.610	0.604	0.582	0.556	0.532	0.531	0.532	0.542	0.553	0.587	0.581	0.598	0.618	0.635	0.666	0.686	0.676	0.667	0.663	0.652	0.647	0.636	RHmix		
73.1	74.2	75.5	76.7	77.8	78.8	79.7	80.3	80.8	80.9	80.6	79.9	78.7	77.1	75.5	73.8	72.2	71.0	70.3	70.0	70.1	70.6	71.2	72.1	Tmix		
0.011	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.013	0.012	0.012	0.012	0.012	0.012	0.012	0.011	0.011	0.011	0.011	0.011	0.011	Wmix	60% OA	
0.653	0.650	0.629	0.620	0.593	0.562	0.534	0.533	0.533	0.545	0.558	0.574	0.592	0.614	0.638	0.659	0.699	0.723	0.712	0.701	0.696	0.683	0.676	0.662	RHmix		
72.8	74.1	75.6	77.0	78.3	79.5	80.5	81.2	81.7	81.9	81.6	80.7	79.3	77.5	75.6	73.6	71.8	70.4	69.5	69.2	69.3	8.69	70.6	71.6	Tmix		
0.012	0.012	0.012	0.013	0.013	0.012	0.012	0.012	0.012	0.013	0.013	0.013	0.013	0.013	0.012	0.012	0.012	0.012	0.012	0.011	0.011	0.011	0.011	0.011	VVmix	70% OA	
0.677	0.673	0.647	0.636	0.605	0.569	0.535	0.534	0.535	0.547	0.562	0.581	0.603	0.628	859.0	0.684	0.732	0.762	0.750	0.737	0.731	0.714	0.706	0.689	RHmix		
72.4	74.0	75.6	77.2	78.8	80.1	81.2	82.1	82.7	82.8	82.5	81.5	79.9	77.8	75.6	73.4	71.3	69.7	68.7	68.4	5.88	69.1	70.0	71.1	Tmix	9	
0.012	0.012	0.013	0.013	0.013	0.013	0.012	0.013	0.013	0.013	0.013	0.014	0.013	0.013	0.013	0.012	0.013	0.012	0.012	0.011	0.011	0.011	0.012	0.012	Wmix	80% OA	
0.702	0.696	0.665	0.652	0.615	0.574	0.537	0.534	0.535	0.549	0.566	0.588	0.613	0.643	0.678	0.709	0.766	0.803	0.789	0.774	0.767	0.747	0.737	0.717	RHmix		
72.1	73.8	75.7	77.5	79.2	80.8	82.0	83.0	83.6	83.8	83.5	82.3	80.5	78.2	75.7	73.2	70.9	69.1	67.9	67.5	67.7	68.3	69.3	70.6	Tmix	3	
0.012	0.013	0.013	0.013	0.013	0.013	0.013	0.013	0.013	0.014	0.014	0.014	0.014	0.014	0.013	0.013	0.013	0.013	0.012	0.012	0.012	0.012	0.012	0.012	Wmix	90% OA	
0.727	0.720	0.683	0.667	0.626	0.579	0.538	0.535	0.535	0.551	0.569	0.594	0.622	0.657	0.698	0.735	0.801	0.845	0.830	0.812	0.804	0.781	0.768	0.745	RHmix		
71.8	73.7	75.8	77.8	79.7	81.4	82.8	83.9	84.6	84.8	84.4	83.1	81.1	78.5	75.8	73.0	70.4	68.4	67.1	66.7	66.9	67.6	68.7	70.1	Tmix	1.	
0.013	0.013	0.013	0.014	0.014	0.013	0.013	0.013	0.014	0.014	0.014	0.015	0.014	0.014	0.014	0.013	0.013	0.013	0.012	0.012	0.012	0.012	0.012	0.012	VVmix	00% OA	
0.753	0.743	0.702	0.683	0.636	0.584	0.538	0.535	0.535	0.552	0.572	0.599	0.631	0.670	0.717	0.761	0.837	0.888	0.872	0.852	0.843	0.816	0.801	0.774	RYMix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	Hour		
74.4	74.6	74.8	75.1	75.2	75.4	75.5	75.6	75.6	75.6	75.4	75.2	74.9	74.6	74.3	74.0	73.8	73.7	73.6	73.6	73.7	73.8	74.0	74.2	Tmix		
0.010	0.010	0.010	0.010	2 0.010	0.010	0.010	0.010	0.010	0.010	0.010	2 0.010	0.010	8 0.010	0.010	0.01	8 0.010	7 0.010	0.009	0.009	7 0.009	0.010	0.010	0.010	x Wmix	Minimum	
0 0.534	0 0.533	0 0.532	0 0.529	0 0.525	0 0.519	0 0.517	0 0.5	0 0.516	0.5	0 0.517	0 0.519	0 0.522	0 0.524	0 0.529	0 0.533	0 0.537	0 0.538	19 0.537	19 0.536	19 0.536	0 0.535	0 0.535	0 0.534	ix RHmix	n OA	
4 74.4	74	12 74.1	9 75.	5 75.	9 75.	7 75.	5 75.1	6 75.	16 75.1	7 75.	9 75.	2 74.	4 74.1	9 74.	13 74.1	73.1	18 73.1	17 73.1	16 73.6	16 73.	15 73.1	5 74.1	14 74.2	iix Tmix		
4 0.010	.6 0.010	3 0.010	1 0.010	3 0.010	4 0.010	3 0.010	3 0.010	7 0.010	3 0.010	5 0.010	2 0.010	0.010	3 0.010	3 0.010	0.010	3 0.010	3 0.010	3 0.009	3 0.009	7 0.009	8 0.010	0.010	2 0.010	× Wmix	10% OA	
0 0.535	0 0.534	0 0.533	0 0.530	0 0.525	0 0.519	0 0.517	0 0.5	0 0.516	0 0.517	0 0.517	0 0.519	0 0.522	0 0.525	0 0.529	0 0.533	0 0.537	0 0.539	19 0.538	19 0.537	19 0.537	0 0.536	0 0.535	0 0.535	ix RHmix	OA	
35 73.7	74.2	3 74.7	75.	5 75.	9 75.8	7 76.	5 76.3	6 76.3	7 76.2	7 75.9	9 75.	2 74.9	5 74.2	73.6	73.0	§7 72.5	19 72.2	18 72.	87 72.2	§7 72.	16 72.6	15 72.9	15 73.3	iix Tmix		
7 0.010	2 0.010	7 0.01	0.010	5 0.010	8 0.010	0.010	8 0.010	8 0.010	2 0.010	0.010	1 0.010	0.010	2 0.010	8 0.010	0.010	5 0.010	2 0.009	0.009	2 0.009	8 0.009	0.009	0.010	8 0.010	x Wmix	20% OA	
0 0.554	0 0.552	0 0.551	0 0.544	0 0.534	0 0.522	0.5	0.5	0 0.517	0 0.517	0.5	0 0.522	0 0.528	0 0.534	0 0.543	0 0.552	0.580	9 0.584	9 0.561	9 0.559	9 0.560	9 0.557	0 0.556	0 0.555	ix RHmix)A	
4 73.1	2 73.8	1 74.5	4 75.2	4 75.8	2 76.3	18 76.7	15 76.9	7 77.0	7 76.8	19 76.4	2 75.7	8 74.8	4 73.8	3 72.8	2 72.0	0 71.3	4 70.8	1 70.7	9 70.7	0 71.0	7 71.3	6 71.9	5 72.5	iix Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.01	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	< Wmix	30% OA	
0 0.574	0 0.57	0.568	0.558	0.543	0 0.526	0.519	0 0.514	0 0.517	0.518	0 0.521	0 0.525	0.535	0.543	0.557	0 0.57	0.584	9 0.591	9 0.586	0.583	9 0.583	9 0.579	0 0.577	0.575	x RHmix)A	
4 72.5	1 73.4	8 74.4	8 75.2	3 76.0	3 76.7	3 77.2	4 77.5	77.6	8 77.4	1 76.8	5 75.9	5 74.7	3 73.4	7 72.1	71.0	4 70.0	1 69.4	69.2	8 69.3	89.6	70.1	70.8	5 71.6	ix Tmix		
0.010	0.010	0.01	0.01	0.01	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	: Wmix	40% OA	
0.595	0.591	0.586	0.572	0.552	0.529	0.519	0.513	0.517	0.518	0.522	0.529	0.541	0.553	0.572	0.591	0.609	0.618	0.611	0.807	0.608	0.602	0.599	0.597	RHmix	Α	
71.8	73.0	74.2	75.3	76.3	77.1	77.8	78.2	78.3	78.0	77.3	76.1	74.7	73.0	71.4	70.0	8.88	0.88	67.8	67.9	68.3	68.9	69.8	70.8	x Tmix		
0.010	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	50% OA	August
0.617	0.611	0.604	0.586	0.561	0.531	0.520	0.512	0.516	0.518	0.523	0.532	0.548	0.563	0.587	0.612	0.636	0.647	0.638	0.633	0.634	0.626	0.623	0.619	RHmix	Д	1
71.2	72.6	74.0	75.4	76.6	77.5	78.3	78.8	78.9	78.6	77.7	76.3	74.6	72.6	70.7	68.9	67.6	66.7	66.4	66.5	67.0	67.7	68.7	69.9	Tmix		
0.010	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	60% OA	
0.639	0.631	0.622	0.600	0.569	0.534	0.520	0.511	0.516	0.518	0.524	0.535	0.554	0.573	0.602	0.633	0.663	0.678	0.667	0.660	0.661	0.651	0.647	0.642	RHmix	,	
70.6	72.2	73.9	75.4	76.8	77.9	78.9	79.4	79.6	79.2	78.2	76.5	74.5	72.2	70.0	67.9	66.3	65.3	64.9	65.1	65.6	66.5	67.7	69.1	Tmix		
0.011	0.011	0.011	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	70% OA	
0.662	0.652	0.641	0.614	0.577	0.537	0.520	0.510	0.515	0.518	0.525	0.538	0.561	0.583	0.618	0.656	0.692	0.711	0.697	0.688	0.690	0.677	0.672	0.666	RHmix		
70.0	71.8	73.7	75.5	77.1	78.4	79.4	0.08	80.2	79.8	78.6	76.8	74.4	71.8	69.2	66.9	65.1	63.9	63.5	63.6	64.3	65.2	66.6	68.2	Tmix		
0.011	0.011	0.012	0.012	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	80% OA	
0.685	0.673	0.659	0.628	0.585	0.539	0.520	0.508	0.515	0.518	0.526	0.540	0.567	0.593	0.635	0.679	0.723	0.745	0.728	0.718	0.720	0.705	0.698	0.691	RHmix		
69.3	71.4	73.6	75.5	77.3	78.8	0.08	80.7	80.9	80.4	79.1	77.0	74.4	71.4	68.5	65.9	63.8	62.5	62.0	62.2	62.9	64.0	85.6	67.4	Tmix		
0.011	0.011	0.012	0.012	0.012	0.011	0.011	0.011	0.012	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	90% OA	
0.709	0.694	0.678	0.642	0.593	0.541	0.520	0.507	0.514	0.517	0.527	0.543	0.574	0.603	0.652	0.703	0.754	0.781	0.761	0.749	0.751	0.734	0.726	0.717	RHmix		
68.7	71.0	73.4	75.6	77.6	79.2	80.5	81.3	81.5	81.0	79.5	77.2	74.3	71.0	67.8	64.9	62.6	61.1	60.6	8.08	61.6	62.8	64.5	6.88	Tmix	1	
0.011	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.012	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	100% OA	
0.734	0.716	0.697	0.855	0.601	0.543	0.520	0.505	0.513	0.516	0.528	0.546	0.581	0.614	0.669	0.728	0.788	0.819	0.796	0.782	0.785	0.764	0.755	0.744	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	80	7	6	5	4	S	2	1	Hour		
73.9	74.1	74.4	74.6	74.8	74.9	75.1	75.2	75.2	75.3	75.2	74.9	74.6	74.1	73.7	73.3	73.1	73.0	73.0	73.1	73.2	73.3	73.5	73.7	Tmix		
0.009	0.009	0.010	8 0.010	0.010	0.010	0.009	2 0.009	2 0.00	0.009	2 0.009	0.009	0.009	0.009	7 0.009	0.009	0.009	0.009	0.009	0.009	2 0.009	0.009	0.009	7 0.009	x Wmix	Minimum	
0.530	0.529	10 0.527	10 0.525	10 0.521	10 0.516	0.509	0.507	0.508	0.507	0.510	0.512	0.517	0.521	0.525	0.530	0.536	0.538	0.538	0.537	19 0.536	0.535	0.533	0.531	iix RHmix	m OA	
73	29 74.	27 74.	25 74.	21 74.	16 74.	J9 75.	J7 75.	18 75.	J7 75.	10 75.	12 74.	17 74.	21 74.	25 73.	30 73.	36 73.	38 72.	38 72.	37 73.	36 73.	35 73.	33 73.	31 73.	nix Tmix		
.9 0.009	1 0.0	3 0.010	6 0.010	8 0.010	9 0.010	1 0.0	2 0.009	3 0.0	3 0.0	2 0.009	9 0.009	6 0.0	1 0.009	7 0.009	3 0.0	0.009	9 0.009	9 0.0	0.009	1 0.0	3 0.0	4 0.0	7 0.0	ix Wmix	10% OA	
09 0.531	.009 0.529	10 0.528	10 0.525	10 0.522	10 0.51	.009 0.5	0	.009 0.5	.009 0.5		09 0.512	.009 0.5	09 0.521	09 0.525	.009 0.531	09 0.537	09 0.539	.009 0.538	09 0.538	.009 0.5	.009 0.536	.009 0.533	.009 0.531	nix RHmix	OA	
31 72.7		28 73.	25 74.	22 74	16 74	.509 75.	.507 75	.507 75	.507 75	.510 75	12 74).517 74.1		25 72	31 71	37 71	39 70	38 70	38 71).537 71	36 71	33 71	31 72	mix Tmix		
	73.2 0.1	7 0		Ċħ	.0	1	.4	.5	.5 0	.4	.9	0	73.2 0.1	ω	.5 0.1	.0 0.1	80	.9 0	.0 0.1	.2 0.1	Ċħ	.9 0.1	ω		20%	
0.009 0.	.009 0.	.010 0.	0.010 0.	0.010 0.	0.009 0.	.009 0.	.009 0.	.009 0.	.009 0.	.009 0.	0.009 0.	.009 0.	0.009 0.	0.009 0.	.009 0.	0.009 0.	0.009 0.	.009 0.	0.009 0.	0.009 0.	0.009 0.	0.009 0.	0.009 0.	Wmix RH	20% OA	
0.547 7	0.543 7	0.540 7	0.535 7	0.528 7	.516 7	.502 7	0.498 7).499 7	0.498 7	.504 7	.508 7	.518 7	1.527 7).535 7	1.547 6	1.558 6	1.564 6).562 6	1.562 6	0.558 6).557 6	0.552 7	0.548 7	RHmix T		
71.6 0	72.3 0	73.0 0	73.7 0	74.3 0	74.8 0	75.2 0	75.5 0	75.8 0	75.8 0	75.5 0	74.8 0	73.7 0	72.3 0	71.0 0	69.8 0	69.0 0	0 8.89	0 8.89	69.0 0	69.4 0	69.8 0	70.3 0	71.0 0	Tmi× ₩	30	
.009 0	.009 0	.010 0	0.010 0	0.010 0	.009 0	.009 0	0.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	.009 0	Wmix R	30% OA	
0.563	.558	.552	.545	.534	515	.495	.489	.491	.489	.498	.504	.519	.532	.544	.562	.581	0.589	.587	.586	.581	.579	.570	0.584	RHmix		
70.5	71.4	72.3	73.2	74.0	74.7	75.3	75.7	76.0	76.1	75.7	74.7	73.2	71.4	69.69	68.1	67.0	66.7	66.8	67.0	67.5	68.1	8.88	9.69	Tmix '	4(
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	40% OA	
0.580	0.573	0.565	0.555	0.540	0.515	0.488	0.480	0.483	0.481	0.492	0.500	0.520	0.538	0.554	0.579	0.604	0.616	0.613	0.612	0.605	0.603	0.590	0.582	RHmix		
69.4	70.5	71.7	72.8	73.8	74.7	75.3	75.9	76.3	76.3	75.9	74.7	72.8	70.5	68.3	66.4	65.0	64.6	64.7	65.0	65.6	66.4	67.2	88.3	Tmix	c n	Se
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.009	0.009	0.009	Wmix	50% OA	Septembe
0.597	0.589	0.578	0.585	0.546	0.515	0.481	0.471	0.475	0.472	0.486	0.496	0.521	0.543	0.563	0.595	0.629	0.645	0.641	0.639	0.630	0.627	0.610	0.600	RHmix		Г
68.2	69.6	71.0	72.3	73.5	74.6	75.4	76.1	76.5	76.6	76.1	74.6	72.3	8.68	66.9	64.6	63.1	62.5	62.6	63.1	63.7	64.6	65.6	66.9	Tmix		
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.009	Wmix	60% OA	
0.615	0.605	0.592	0.575	0.552	0.515	0.474	0.462	0.467	0.464	0.480	0.492	0.522	0.548	0.572	0.612	0.654	0.674	0.669	0.667	0.655	0.652	0.632	0.618	RHmix		
67.1	68.7	70.3	71.9	73.3	74.5	75.5	76.3	76.8	76.9	76.3	74.5	71.9	68.7	65.6	62.9	61.1	60.4	60.6	61.1	61.8	62.9	64.1	65.6	Tmix		
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.009	Wmix	70% OA	
0.634	0.621	0.606	0.586	0.559	0.515	0.468	0.454	0.459	0.456	0.475	0.488	0.523	0.553	0.581	0.629	0.681	0.705	0.699	0.697	0.682	0.678	0.653	0.638	RHmix		
66.0	67.8	69.6	71.4	73.0	74.4	75.6	76.4	77.0	77.2	76.4	74.4	71.4	67.8	64.2	61.2	59.1	58.4	5.83	59.1	0.08	61.2	62.5	64.2	Tmix		
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.007	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	80% OA	
0.654	0.638	0.620	0.597	0.565	0.515	0.461	0.445	0.452	0.448	0.469	0.484	0.523	0.559	0.590	0.646	0.708	0.738	0.730	0.728	0.710	0.706	0.676	0.857	RHmix	ш	
64.8	66.9	69.0	71.0	72.8	74.4	75.6	76.6	77.3	77.4	76.6	74.4	71.0	66.98	62.9	59.4	57.1	56.3	56.5	57.1	58.1	59.4	61.0	62.9	Tmix		
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.008	0.008	0.008	0.008	0.008	Wmix	90% OA	
0.674	0.656	0.635	0.608	0.572	0.515	0.454	0.437	0.444	0.440	0.463	0.480	0.524	0.563	0.599	0.663	0.736	0.772	0.763	0.760	0.739	0.735	0.700	0.678	RHmix	Þ	
63.7	0.88	68.3	70.5	72.5	74.3	75.7	76.8	77.5	77.7	76.8	74.3	70.5	0.33	61.5	57.7	55.1	54.2	54.4	55.1	56.2	57.7	59.4	81.5	× Tmix		
0.009	0.009	0.010	0.010	0.010	0.009	0.008	0.008	0.009	0.009	0.009	0.009	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	0.008	0.008	< Wmix	100% OA	
9 0.695	9 0.674	0.650	0 0.619	0 0.578	9 0.515	8 0.447	8 0.428	9 0.437	9 0.432	9 0.458	9 0.475	8 0.524	8 0.568	7 0.607	7 0.680	7 0.765	7 0.808	7 0.797	7 0.794	7 0.770	8 0.765	8 0.724	8 0.699	x RHmix	OA	
ői	4	ő	9	ωŏ	O	7	ŏ	7	Ñ	ő	ŰĬ	24	őő	17	ő	őί	60	17	Z	Ö	Űń	4	Ö	×		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	80	7	6	5	4	з	2	1	Hour		
72.6	72.9	73.1	73.3	73.5	73.6	73.7	73.8	73.8	73.7	73.6	73.3	72.9	72.6	72.2	71.9	71.8	71.7	71.7	71.8	71.9	72.0	72.2	72.4	Tmix		
0.009	0.009	0.00	0.009	5 0.009	0.00	7 0.009	0.009	0.00	7 0.009	0.009	0.009	0.009	0.009	2 0.009	0.009	8 0.009	7 0.009	7 0.009	0.009	0.009	0.009	2 0.009	0.009	x Wmix	Minimum	
19 0.536	9 0.534	19 0.532	19 0.529	9 0.528	9 0.523	9 0.517	0.5	19 0.515	0.5	0.5	9 0.520	9 0.525	19 0.531	9 0.536	19 0.540	19 0.544	19 0.545	19 0.544	19 0.543	19 0.543	9 0.542	9 0.540	19 0.539	ix RHmix	n OA	
36 72.6	34 72.1	12 73.1	73.	28 73.	73.1	7 73.	16 73.	5 73.1	16 73.	18 73.	20 73.	25 72.1	31 72.5	36 72.1	10 71.1	71.6	15 71.1	71.6	13 71.7	13 71.1	12 71.9	10 72.1	39 72.3	nix Tmix		
3 0.009	8 0.009	0.009	2 0.009	4 0.009	3 0.009	7 0.009	7 0.009	3 0.009	7 0.009	5 0.009	2 0.009	0.009	5 0.009	1 0.009	3 0.009	3 0.009	3 0.009	3 0.009	7 0.009	3 0.009	0.009	1 0.009	3 0.009	× Wmix	10% OA	
19 0.537	19 0.535	19 0.532	19 0.530	19 0.528	19 0.523	19 0.517	19 0.51	19 0.515	19 0.51	19 0.51	19 0.520	19 0.525	19 0.531	19 0.537	19 0.541	19 0.545	19 0.546	19 0.546	19 0.545	19 0.544	19 0.543	19 0.541	9 0.539	iix RHmix	OA	
37 70.1	35 70.	32 71.	30 71.4	28 71.	23 72.	72.	6 72.	5 72.	6 72.4	8 72.	20 71.4	25 70.	89.9	37 69.	68	15 88.	188 88	16 68.	15 68.	88	68	11 69.	69	nix Tmix		
1 0.009	6 0.009	0 0.009	4 0.009	8 0.009	1 0.009	3 0.009	5 0.009	5 0.009	4 0.009	0 0.009	4 0.009	7 0.009	9 0.008	2 0.008	.6 0.008	3 0.008	1 0.008	2 0.008	3 0.008	.6 0.009	.9 0.009	2 0.009	.6 0.009	ix Wmix	20% OA	
19 0.558	19 0.554	19 0.549	19 0.545	19 0.54	19 0.531	0.5	0.5	19 0.513	0.5	19 0.520	19 0.524	19 0.534	0.546	18 0.558	0.568	18 0.576	18 0.577	18 0.577	18 0.574	19 0.573	19 0.571	19 0.567	19 0.564	ix RHmix	OA	
8 67.7	4 68.3	9 69.0	5 69.6	1 70.2	70.	18 71.1	15 71.2	3 71.3	16 71.	0 70.5	4 69.6	68.6	6 67.4	66.3	8 65.5	64.9	7 64.7	7 64.8	4 65.0	3 65.3	1 65.8	7 66.3	4 67.0	iix Tmix		
7 0.008	3 0.008	0.00	3 0.009	2 0.00	7 0.00	0.008	2 0.00	3 0.00	1 0.008	5 0.008	3 0.008	3 0.008	4 0.008	3 0.008	5 0.008	0.008	7 0.008	0.008	0.008	3 0.008	0.008	8 0.008	0.008	× Wmix	30% OA	
8 0.580	8 0.574	9 0.566	9 0.559	9 0.553	9 0.538	0.5	8 0.51	8 0.510	8 0.514	8 0.521	8 0.527	8 0.541	8 0.560	8 0.578	8 0.594	8 0.607	8 0.609	8 0.609	8 0.605	8 0.603	8 0.599	8 0.593	8 0.589	ix RHmix)A	
0 65.2	4 66.1	6 67.0	9 67.8	3 68.6	8 69.2	9.69	4 69.9	0 70.0	4 69.8	1 69.0	7 67.8	1 66.4	0 64.9	8 63.4	4 62.3	7 61.5	9 61.3	9 61.4	5 61.6	3 62.1	9 62.7	8 63.4	9 64.3	iix Tmix		
2 0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	0.008	0.008	0.008	< Wmix	40% OA	
8 0.602	8 0.594	8 0.583	8 0.574	8 0.566	8 0.544	8 0.517	8 0.511	8 0.506	8 0.512	8 0.520	8 0.529	8 0.548	7 0.573	7 0.598	7 0.621	7 0.639	7 0.642	7 0.641	7 0.636	8 0.634	8 0.629	8 0.620	8 0.615	× RHmix	DA	
2 62.8	63.9	85.0	1 66.0	67.0	67.8	7 68.3	88.6	8.89	88.5	87.5	66.0	64.3	82.4	80.5	59.1	58.1	2 57.9	58.0	58.3	9.85	59.6	60.5	61.6	× Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.008	0.00	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	: Wmix	50% OA	October
0.624	0.614	0.601	0.589	0.579	0.551	0.516	0.508	0.501	0.509	0.519	0.529	0.552	0.585	0.617	0.647	0.672	0.675	0.674	0.667	0.665	0.658	0.648	0.641	: RHmix	Å	er
60.3	61.7	63.0	64.3	65.3	66.3	67.0	67.4	67.5	67.1	0.88	64.3	62.1	59.8	57.7	55.9	54.8	54.4	54.5	55.0	55.7	56.6	57.7	58.9	< Tmix		
0.007	0.007	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.007	0.007	0.007	0.007	Wmix	60% OA	
0.646	0.634	0.618	0.604	0.592	0.556	0.513	0.503	0.495	0.504	0.516	0.527	0.555	0.595	0.635	0.672	0.704	0.708	0.707	0.698	0.695	0.688	0.675	0.668	RHmix	ь	
57.9	59.5	61.0	62.5	63.7	64.9	65.6	66.1	66.3	8.38	64.5	62.5	60.0	57.3	54.8	52.7	51.4	51.0	51.1	51.6	52.5	53.5	54.8	56.2	Tmix		
0.007	0.007	0.007	0.007	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.007	Wmix	70% OA	
0.668	0.655	0.636	0.618	0.604	0.562	0.509	0.498	0.487	0.499	0.512	0.523	0.555	0.603	0.650	0.696	0.735	0.739	0.739	0.727	0.726	0.717	0.702	0.694	RHmix		
55.4	57.2	59.0	60.7	62.1	63.4	64.3	84.8	65.0	84.5	63.0	60.7	57.8	54.8	51.9	49.6	48.0	47.6	47.7	48.3	49.2	50.4	51.9	8.85	Tmix		
0.006	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.006	0.006	0.008	Wmix	80% OA	
0.690	0.675	0.653	0.633	0.617	0.566	0.504	0.491	0.478	0.492	0.506	0.517	0.553	0.607	0.663	0.716	0.764	0.769	0.768	0.755	0.754	0.745	0.728	0.721	RHmix		
53.0	55.0	57.0	58.9	60.5	62.0	62.9	63.6	63.8	63.2	61.5	58.9	55.7	52.2	49.0	46.4	44.7	44.1	44.3	44.9	46.0	47.4	49.0	50.9	Tmix		
0.006	0.006	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.006	Wmix	90% OA	
0.712	0.695	0.670	0.647	0.629	0.570	0.497	0.483	0.468	0.483	0.499	0.509	0.548	0.609	0.671	0.734	0.791	0.796	0.795	0.779	0.781	0.772	0.753	0.746	RHmix		
50.5	52.8	55.0	57.1	68.9	60.5	61.6	62.3	62.5	61.9	0.08	57.1	53.5	49.7	46.1	43.2	41.3	40.7	40.9	41.6	42.8	44.3	46.1	48.2	Tmix	1	
0.006	0.006	0.006	0.007	0.007	0.006	0.006	0.006	0.005	0.006	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.005	0.005	0.005	0.005	Wmix	00% OA	
0.732	0.714	0.686	0.661	0.641	0.573	0.489	0.473	0.456	0.473	0.489	0.498	0.539	0.806	0.675	0.746	0.813	0.817	0.817	0.799	0.804	0.796	0.776	0.771	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	Hour		
72.0	72.3	72.5	72.7	72.8	73.0	73.	73.2	73.2	73	72.9	72.7	72.3	72.0	71.1	71.4	71.3	71.	71.	71.5	71.3	71.5	71.6	71.8	Tmix		
0.009	3 0.009	5 0.009	7 0.009	8 0.009	0.009	0.009	2 0.009	2 0.009	0.009	0.009	7 0.009	3 0.009	0.009	3 0.009	4 0.009	2 0.009	0.009	1 0.009	2 0.009	3 0.009	5 0.009	3 0.009	8 0.009	× Wmix	Minimum OA	
19 0.538	0.537	0.535	0.534	0.532	0.529	0.525	0.522	0.521	0.522	0.524	0.528	0.531	0.536	0.541	0.546	0.548	0.548	0.548	0.547	0.546	0.545	0.543	0.541	iix RHmix	m OA	
38 71.9	87 72	35 72	34 72.6	32 72	29 72	25 73	22 73.	21 73.	22 73.	24 72.9	28 72.6	81 72	36 71.9	11 71.5	16 71.2	71.0	18 71	18 71.0	71.1	16 71	15 71.3	13 71.5	11 71.7	nix Tmix		
9 0.009	2 0.009	4 0.0	6 0.009	8 0.009	9 0.0	0.009	1 0.009	1 0.0	1 0.009	9 0.009	6 0.009	2 0.0	9 0.009	5 0.009	2 0.009	0 0.009	0 0.009			2 0.009	0		7 0.009	ix Wmix	10% OA	
09 0.539	09 0.538	.009 0.535	09 0.535	09 0.533	.009 0.530	09 0.526	09 0.522	.009 0.5	09 0.522	09 0.524	09 0.528	.009 0.532	09 0.537	09 0.542	09 0.547	09 0.549	09 0.549	.009 0.550	.009 0.548	09 0.548	.009 0.546	.009 0.5	09 0.542	nix RHmix	OA	
88	38 69	35 69	35 70.	33 70	30 70	26 71	22 71	.521 71	22 71	24 70.	28 70.	32 69	37 68.7	42 68	47 67.4	49 67.0	66	67	48 67.1	48 67	67	.544 68	42 68	mix Tmix		
.8 0.008	.3 0.009	.7 0	.1 0.009	.5 0.009	.8 0	.0 0.009	.2 0.009	.2 0.009	.1 0.009	.7 0.008	.1 0.008	.4 0.008	.7 0.008	.0 0.008	.4 0.008	.0 0.008	.9 0.008	.0 0.008	.1 0.008	.3 0.008	.6 0.008	.0 0.008	.4 0.008	nix Wmix	20% OA	
0.563	_	.009 0.6	0.555	_	.009 0.6		_		09 0.527	_	_	_	_	_	_	0.584	_	_	08 0.582	0.581	08 0.577	08 0.573	0.568	nix RHmix	OA	
65.8	0.560 66.	0.555 67.1	55 87.7	0.550 68.).544 68.	0.535 89.).528 69.	1.525 69.3	27 69.2	0.531 68.6	0.539 67.7	0.548 66.	0.558 85.6).569 64.5	0.579 63.6	84 63.	1.583 62.9).584 62.9	82 63.2	81 63.5	77 63.9	73 64.5	68 65.	mix Tmix		
	5 0		.7 0.008	3 0	7 0	1 0	.3 0.008		0	800.0	0	7 0	0			.1 0.008	0		0	0	0		_		30% OA	
.008 0.587	.008 0.582	.008 0.6	0	.008 0.5	.008 0.5	.008 0.5	0	.008 0.6	.008 0.5		.008 0.5	.008 0.6	.008 0.5	.008 0.5	.008 0.6	3.0 800	.008 0.8	.008 0.6	.008 0.6	.008 0.6	.008 0.8	.008 0.8	0.008 0.595	Wmix RH	OA	
Н	63	.575 64	.575 65	.567 66	.557 66	.544 6	.533 6	.528 67	.531 6	.538 66	.550 65	.562 63	.578 62	.595 6	.611 59	519 59	.617 58	.620 58	.616 5	.614 59	.609 61	.602 6		RHmix Ti		
62.7 0.1	9	Ü	ω	-	0 9	67.1 QJ	67.4 O.I	4 0	67.2 QJ	4	ω	.9 0	4	61.0 0.1	. 8	_	00	9 0	59.2 O.I	0 9	60.2 0.1	61.0 0.1	61.8 0.1	Tmix W	40%	
0.007 0.	0.008 0.	0.008 0.	0.008 0.	0.008 0.	.008 0.	0.008 0.	0.008 0.	.008 0.	0.008 0.	0.007 0.	0.007 0.	.007 0:	0.007 0.	0.007 0.	.007 0.	0.007 0.	0.007 0.	.007 0.	.007 0.	.007 0.1	.007 0.	.007 0.	.007 0.	Wmix RH	40% OA	
0.611 59	0.603 60	0.594 61	0.594 62	0.584 63).570 64	0.552 85	0.537 65	0.530 65	0.534 65	0.542 64	0.559 62	0.575 6	0.597 5	0.621 57	0.643 56	0.654 5	0.651 54	0.655 54	0.650 55	0.647 55	0.640 56	0.631 57	0.622 58	RHmix T		
Ö	.00	.9 0	9	œ	.5 0	_	Ç,	Ċħ	ω	ω	9	61.1 0.	59.3 0.	Ċħ	0	55.1 0.	00	9	ω	œ	Ċħ	Ö	5	Tmix W	509	Novi
0.007 0.	0.007 0.	.007 0.	0.007 0.	0.008 0.	1.008 0.	0.007 0.	0.007 0.	0.007 0.	0.007 0.	0.007 0.	0.007 0.	0.007 0.	0.007 0.	0.006 0.	0.006 0.	0.006 0.	0.006 0.	0.006 0.	0.006 0.	0.006 0.	0.006 0.	0.007 0.	0.007 0.	Wmix RH	50% OA	Vovember
0.633 5	0.625 5).613 5	0.614 8	.600 8	1.583 6	1.559 6	0.539 6).530 6	0.535 6).545 B	0.565 6	0.586 5	0.614 5	1.645 5	0.673 5	1.688 5	.683 5	.690 5	0.683 5	1.679 5	0.671 5	0.660 5	0.647 5	RHmix T		
56.5 0.	57.9 0.	59.2 0.	60.4 0.	61.6 0.	62.5 0.	63.1 0.	63.5 0.	63.7 0.	63.3 0.	62.2 0.	60.4 0.	58.3 0.	56.1 0.	54.0 0.	52.3 0.	51.1 0.	50.8 0.	50.9 0.	51.3 0.	52.0 0.	52.9 0.	54.0 0.	55.2 0.	Tmix W	609	
.006 0	007 0	007 0	0.007 0	.007 0	.007 0	007 0	0.007 0	.007 0	.007 0	0.006 0	0.006	.006 0	.006 0	.006 0	.006 0	0.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	0.006 0	Wmix RI	60% OA	
0.655 6	0.645 6	.631 6	.634	.617 6	.595 6	.564 6	0.539 6	.528 E	.534 E	.546 E	.570 6	.595 6	.629 6	.667 6	.702 4	0.720 4	0.713 4	.722 4	0.713 4	0.710 4	.699 4	.686	0.671 6	RHmix T		
53.4 0	55.1 0	56.6 0	58.0 0	59.3 0	60.4 0	11.1 0	61.6 0	61.8 0	61.4 0.	0.00	58.0 0.	55.5 0	53.0 0	50.5 0	48.5 0	47.1 0	46.7 0	46.9 0	47.4 0	48.1 0	49.2 0.	50.5 0.	51.9 0	Tmi× ₩	70%	
0.006 0	.006 0	.006 0	0.007 0	007 0	.007 0	.006 0	0 900	.006 0	900	0.006 0	900	.006 0	0.005 0	.005 0	.005 0	0.005 0	0.005 0	0.005 0	0.005 0	0.005 0	005	900	0.008 0	Wmix R	% OA	
0.674	0.663 4	0.648 8	0.652	0.632	0.606 6	0.568	0.537	0.524	0.530	0.544	0.572	0.600 6	0.639	0.684	0.727 4	0.748	0.738 4	0.750 4	0.739 4	0.737 4	0.725	0.710 4	0.693 4	RHmix		
50.4 0	52.2 0	54.0 0	55.6 0	57.1 0	58.3 0	59.2 0	59.7 0	9.9 0	59.4 0	57.9 0	55.6 0	52.8 0	49.8 0	47.0 0	44.7 0	43.2 0	42.7 0	42.8 0	43.4 0	44.3 0	45.5 0	47.0 0	48.6 0	Tmix V	80	
0.005 (0.006 0	0.006 0	0.006 (0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.005 0	0.005 0	0.005 0	0.005 (0.005 0	0.005 0	0.005 (0.004 (0.004 0	0.004 0	0.005 0	0.005 0	0.005 0	0.005 (Wmix F	80% OA	
0.690	0.680	0.662	0.671	0.647	0.616	0.571	0.534	0.517	0.524	0.539	0.571	0.601	0.645	0.697	0.747	0.770	0.755	0.771	0.759	0.758	0.746	0.731	0.712	RHmix		
47.3 (49.4 (51.3	53.1	54.8	56.2 (57.2	57.8 (58.0 0	57.5	55.7 (53.1 (50.0 (48.7 (43.5	40.9 (39.2	38.6 (38.8	39.5	40.4	41.8 (43.5	45.3 (Tmix \	90	
0.005	0.005	0.005	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.005	Wmix F	90% OA	
0.703	0.694	0.675	0.688	0.661	0.625	0.571	0.527	0.507	0.516	0.531	0.565	0.596	0.644	0.702	0.759	0.783	0.761	0.784	0.770	0.772	0.760	0.745	0.726	RHmix		
44.2	46.5	48.7	50.7	52.6	54.1	55.2	9.35	56.1	55.5	53.6	50.7	47.2	43.5	40.0	37.1	35.2	34.6	34.8	35.5	36.6	38.1	40.0	42.0	Tmix	11.	
0.004	0.005	0.005	0.005	0.006	0.006	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.003	0.003	0.003	0.003	0.004	0.004	0.004	0.004	Wmix F	00% OA	
0.710	0.704	0.685	0.703	0.673	0.631	0.569	0.518	0.494	0.503	0.519	0.555	0.586	0.635	0.697	0.759	0.782	0.753	0.782	0.767	0.774	0.765	0.752	0.733	RHmix		

9% OA 17 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19	AHMIX Trix VMX PHIMIX PLAN 1006 0.778 0.509 0.007 0.630 6.79 0.007 0.630 6.79 0.007 0.680 0.706 0.718 0.509 0.007 0.630 6.79 0.007 0.680 6.29 0.006 0.706 0.504 6.10 0.007 0.630 6.65 0.007 0.680 6.29 0.006 0.708 0.504 6.10 0.007 0.630 6.65 0.007 0.681 5.2 0.006 0.708 0.504 6.10 0.007 0.630 6.65 0.007 0.681 5.1 0.006 0.713 0.508 6.1 0.007 0.630 6.65 0.007 0.681 5.1 0.006 0.721 0.508 6.0 0.07 0.630 6.65 0.007 0.681 5.1 0.006 0.721 0.509 6.0 0.007 0.641 5.6 0.007 0.680 5.1 0.006 0.725 0.509 6.0 0.007 0.643 5.6 0.007 0.684 5.1 0.006 0.725 0.509 6.0 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.0 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.007 0.684 5.1 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.007 0.643 5.2 0.006 0.728 0.509 6.1 0.006 0.728 0.006 0.728 0.00	A 20% OA 10% CA 10% CA 20% CA	A	Color Colo	A 30% CA 40% CA 40% CA 50% CA 60% CA 70% CA 70% CA 80% CA
40% OA Trrix Wrnix 57.8 0.007 57.3 0.007 56.9 0.007 56.3 0.007 56.3 0.007 56.1 0.007 56.1 0.007 56.2 0.007 56.2 0.007 56.3 0.007 56.4 0.007	Timix Vmix RHmix Timix Wmix RHmix 578 0.007 0.688 53.5 0.006 0.706 573 0.007 0.688 52.9 0.006 0.706 580 0.007 0.687 52.9 0.006 0.713 581 0.007 0.687 52.9 0.006 0.713 582 0.007 0.688 51.9 0.006 0.721 583 0.007 0.684 51.4 0.006 0.725 580 0.007 0.684 51.4 0.006 0.728 580 0.007 0.685 51.3 0.006 0.728 580 0.007 0.685 51.3 0.006 0.728 580 0.007 0.685 51.3 0.006 0.728 580 0.007 0.685 51.3 0.006 0.728 580 0.007 0.685 51.3 0.006 0.728 580 0.007 0.685 51.3 0.006 0.728	Trix White RHmix Trix Trix White RHmix Trix Trix Trix White RHmix Trix	Trix Wrink Rehmix Trix Trix Wrink Rehmix Trix Trix Trix Wrink Rehmix Trix Trix	Time: White RHmix Time	Trix Wrink RHmix Trix Wrink RHmix
	December	December	Desember SDR-GAN 70% OA 509% OA 70% OA 70% OA V/mix RHmix T/mx V/mix RHmix 0.006 0.708 49.2 0.005 0.741 44.9 0.005 0.771 0.006 0.716 49.2 0.005 0.747 44.1 0.005 0.771 0.006 0.716 49.2 0.005 0.747 44.1 0.005 0.772 0.006 0.718 47.8 0.005 0.744 42.7 0.004 0.782 0.006 0.719 47.3 0.005 0.756 42.2 0.004 0.782 0.006 0.721 48.8 0.005 0.761 42.0 0.004 0.789 0.006 0.728 48.6 0.005 0.761 42.0 0.004 0.799 0.006 0.728 48.6 0.005 0.761 42.0 0.004 0.799 0.006 0.728	December	December December Bose OA

Appendix C: Air Mixture Results for Water Feature Conditions

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	80	7	6	5	4	ω	2	1	Hour		
70.5	70.6	70.8	70.9	71.1	71.2	71.3	71.4	71.5	71.5	71.5	71.3	71.1	70.8	70.6	70.3	70.1	70.0	69.9	69.9	70.0	70.1	70.2	70.3	Tmix	M	
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	Minimum (
0.552	0.550	0.549	0.546	0.544	0.542	0.540	0.537	0.537	0.536	0.538	0.541	0.544	0.548	0.552	0.554	0.556	0.557	0.559	0.559	0.558	0.557	0.555	0.553	RHmix	OA	
70.3	70.4	70.6	70.8	70.9	71.1	71.2	71.3	71.3	71.4	71.3	71.2	70.9	70.7	70.4	70.1	69.9	8.88	69.7	69.7	8.88	69.9	70.0	70.1	Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	10% 04	
0.553	0.552	0.550	0.547	0.545	0.543	0.541	0.538	0.537	0.537	0.539	0.542	0.545	0.549	0.553	0.556	0.558	0.559	0.561	0.561	0.559	0.558	0.556	0.555	RHmix		
65.5	65.9	66.2	66.6	66.9	67.2	67.4	67.6	67.7	67.7	67.6	67.3	66.9	66.3	65.8	65.2	64.8	64.5	64.4	64.4	64.6	64.7	65.0	65.2	Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	20% OA	
0.591	0.588	0.585	0.579	0.575	0.570	0.565	0.560	0.558	0.558	0.561	0.568	0.573	0.582	0.591	0.597	0.602	0.604	0.607	0.607	0.604	0.602	0.598	0.595	RHmix		
8.08	61.3	61.8	62.4	62.8	63.3	63.6	63.9	64.0	64.1	63.9	63.5	62.8	62.0	61.1	60.4	59.7	59.3	59.1	59.2	59.3	59.6	59.9	60.4	Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	V/mix	30% OA	
0.628	0.624	0.620	0.610	0.603	0.596	0.587	0.579	0.576	0.576	0.581	0.592	0.601	0.615	0.629	0.639	0.646	0.649	0.654	0.654	0.650	0.646	0.639	0.634	RHmix		
56.1	56.8	57.4	58.1	58.8	59.3	59.8	60.2	60.4	60.4	60.2	59.7	58.8	57.7	56.5	55.5	54.6	54.0	53.8	53.9	54.1	54.4	54.9	55.5	Tmix		
0.006	0.006	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	Wmix	40% OA	
0.664	0.658	0.652	0.639	0.629	0.620	0.607	0.595	0.591	0.590	0.599	0.614	0.626	0.646	0.666	0.679	0.688	0.691	0.700	0.699	0.693	0.688	0.678	0.671	RHmix		
51.4	52.2	53.1	53.9	54.7	55.4	56.0	58.5	56.7	56.8	58.5	55.8	54.7	53.4	51.9	50.6	49.5	48.8	48.5	48.6	48.9	49.3	49.9	50.6	Tmix		
0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	Wmix	50% OA	January
0.695	0.688	0.682	0.665	0.652	0.640	0.623	0.606	0.601	0.600	0.612	0.632	0.647	0.674	0.699	0.715	0.725	0.729	0.741	0.740	0.732	0.726	0.713	0.704	RHmix		
46.6	47.7	48.7	49.7	50.7	51.5	52.2	52.7	53.0	53.2	52.9	52.0	50.7	49.0	47.3	45.7	44.4	43.6	43.2	43.3	43.7	44.2	44.9	45.7	Tmix		
0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	V/mix	60% OA	
0.718	0.712	0.708	0.684	0.669	0.654	0.632	0.611	0.604	0.604	0.619	0.645	0.663	0.696	0.726	0.744	0.755	0.757	0.773	0.773	0.762	0.754	0.738	0.728	RHmix		
41.9	43.1	44.3	45.5	46.6	47.6	48.4	49.0	49.4	49.5	49.2	48.2	46.6	44.7	42.7	40.8	39.3	38.3	37.9	38.0	38.5	39.0	39.9	40.8	Tmix		
0.004	0.004	0.004	0.004	0.005	0.005	0.005	0.004	0.004	0.004	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	Wmix	70% OA	
0.730	0.725	0.721	0.696	0.678	0.661	0.634	0.607	0.599	0.600	0.618	0.850	0.670	0.709	0.743	0.761	0.770	0.769	0.790	0.790	0.777	0.768	0.749	0.740	RHmix		
37.2	38.5	39.9	41.3	42.6	43.7	44.6	45.3	45.7	45.9	45.5	44.3	42.6	40.4	38.0	35.9	34.2	33.1	32.7	32.7	33.2	33.9	34.9	36.0	Tmix		
0.003	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	V/mix	80% OA	
0.723	0.723	0.724	0.695	0.675	0.657	0.624	0.592	0.583	0.584	0.607	0.644	0.665	0.708	0.745	0.760	0.763	0.755	0.782	0.782	0.767	0.759	0.738	0.731	RHmix		
32.4	34.0	35.5	37.1	38.5	39.8	40.8	41.6	42.1	42.2	41.8	40.5	38.5	36.1	33.4	31.1	29.1	27.8	27.4	27.5	28.0	28.7	29.8	31.1	Tmix		
0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.003	Wmix	90% OA	
0.690	0.698	0.707	0.676	0.657	0.638	0.599	0.561	0.551	0.553	0.581	0.624	0.643	0.689	0.725	0.735	0.734	0.718	0.754	0.754	0.735	0.726	0.701	0.695	RHmix		
27.7	29.4	31.1	32.8	34.4	35.9	37.0	37.9	38.4	38.6	38.1	36.7	34.5	31.7	28.8	26.2	24.0	22.6	22.1	22.2	22.8	23.6	24.8	26.2	Tmix	1	
0.002	0.002	0.002	0.002	0.003	0.003	0.003	0.002	0.002	0.002	0.003	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	Wmix	100% OA	
0.632	0.650	0.666	0.632	0.616	0.599	0.555	0.510	0.499	0.502	0.536	0.585	0.599	0.645	0.684	0.683	0.658	0.619	0.664	0.865	0.646	0.642	0.621	0.627	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	00	7	8	5	4	з	2	1	Hour		
70.4	70.6	70.7	70.8	71.0	71.1	71.2	71.2	71.3	71.3	71.2	71.1	70.8	70.6	70.3	70.1	69.9	69.9	69.9	69.9	70.0	70.1	70.2	70.3	Tmix	N	
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	Minimum	
0.552	0.551	0.549	0.549	0.546	0.544	0.542	0.540	0.540	0.539	0.541	0.543	0.547	0.550	0.553	0.557	0.559	0.559	0.560	0.559	0.558	0.557	0.556	0.554	RHmix	OA	
70.3	70.4	70.5	70.7	70.8	70.9	71.0	71.1	71.1	71.1	71.1	70.9	70.7	70.4	70.1	69.9	69.7	69.7	69.7	69.7	69.8	69.9	70.0	70.1	Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	10% OA	
0.554	0.552	0.551	0.550	0.547	0.545	0.543	0.541	0.541	0.540	0.542	0.544	0.548	0.551	0.555	0.558	0.561	0.561	0.562	0.561	0.560	0.559	0.558	0.555	RHmix	4	
65.5	85.8	66.1	66.3	8.88	8.33	67.0	67.1	67.2	67.3	67.1	8.33	66.3	85.8	65.3	64.8	64.5	64.4	64.4	64.5	64.6	64.8	65.0	65.3	Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	800.0	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	20% OA	
0.593	0.590	0.586	0.585	0.578	0.574	0.570	0.585	0.565	0.563	0.567	0.572	0.580	0.587	0.594	0.602	0.609	0.609	0.610	0.608	0.606	0.603	0.601	0.596	RHmix		
60.8	61.2	61.6	62.0	62.4	62.7	63.0	63.2	63.3	63.4	63.2	62.7	62.0	61.2	60.4	59.7	59.2	59.1	59.1	59.2	59.4	59.7	60.0	60.4	Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	30% OA	
0.632	0.627	0.621	0.620	809.0	0.601	0.596	0.588	0.587	0.584	0.591	0.597	0.612	0.622	0.634	0.646	0.657	0.657	0.658	0.656	0.653	0.648	0.644	0.636	RHmix		
56.0	56.6	57.2	57.7	58.2	58.7	59.0	59.3	59.4	59.5	59.3	58.7	57.7	56.6	55.5	54.6	53.9	53.7	53.8	53.9	54.2	54.6	55.0	55.5	Tmix	- 4	
0.006	0.006	0.006	0.007	0.007	0.007	0.007	0.006	0.007	0.006	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	Wmix	40% OA	
0.669	0.662	0.655	0.654	0.637	0.627	0.619	0.606	0.606	0.602	0.611	0.621	0.641	0.655	0.671	0.689	0.704	0.704	0.706	0.703	0.698	0.691	0.686	0.675	RHmix		
51.3	52.0	52.7	53.4	54.0	54.6	55.0	55.3	55.5	55.6	55.3	54.6	53.4	52.0	50.7	49.5	48.7	48.4	48.5	48.7	49.0	49.5	50.0	50.7	Tmix	5	F
0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.008	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.006	Wmix F	50% OA	Febuary
0.702	0.694	0.684	0.685	0.662	0.648	0.637	0.621	0.620	0.615	0.627	0.639	0.665	0.683	0.703	0.728	0.748	0.747	0.750	0.746	0.740	0.730	0.725	0.709	RHmix		
46.6 (47.4	48.3	49.0 (49.8	50.5 (51.0 (51.4	51.7	51.8 (51.4 (50.5 (49.0 (47.4 (45.8 (44.4	43.4	43.1 (43.2 (43.4 (43.8 (44.4 0	45.0 (45.8 (Tmix \	60	
0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 (0.005 0	0.005 (0.005 0	0.005 0	0.005 0	0.005 0	0.005 0	0.005	0.005 0	0.005 (Wmix F	60% OA	
0.728	0.719	0.708	0.711	0.681	0.663	0.650	0.628	0.627	0.621	0.637	0.651	0.684	0.704	0.727).758	0.784	0.781	.787	.781	0.773	.762	0.756	0.737	RHmix		
41.8 0	42.8 0	43.8 0	44.7 0	45.6 0	46.4 0	47.0 0	47.5 0	47.8 0	47.9 0	47.5 0	46.4 0	44.7 0	42.8 0	40.9 0	39.3 0	38.1 0	37.8 0	37.9 0	38.1 0	38.6 0	39.3 0	40.0 0	40.9 0	Tmix V	70	
0.004 0	0.004 0	.004 0	.005 0	.004 0	.004 0	.004 0	.004 0	.004 0	.004 0	.004 0	.004 0	.004 0	1.004 0	.004 0	.004 0	1.004 0	.004 0	.004 0	0.004 0	1.004 0	.004 0	.004 0	0.004 0	Wmix R	70% OA	
0.743	0.734 3	0.723	0.729 4	0.691 4	0.670 4	0.653 4	0.625 4	0.625 4	1.617 4	0.637 4	0.653 4	0.692 4	0.713 3	0.739	0.775	0.808	0.800 3	0.809	0.802	0.794	0.780 3	0.775	0.751	RHmix T		
37.1 0	38.2 0	39.3 0	40.4 0	41.4 0	42.3 0	43.0 0	43.5 0	43.9 0	44.0 0	43.5 0	42.3 0	40.4 0	38.2 0	36.1 0	34.2 0	32.9 0	32.5 0	32.6 0	32.9 0	33.4 0	34.2 0	35.0 0	36.0 0	Tmix V	80	
0.003 0.	.004 0	0.004 0.	0.004 0	0.004 0	0.004 0	0.004 0.	0.004 0	0.004 0.	0.004 0	0.004 0	0.004 0	0.004 0.	0.003 0	0.003 0.	0.003 0	0.003 0.	0.003 0	0.003 0.	0.003 0	0.003 0.	0.003 0	0.003 0	0.003 0	Wmix RI	80% OA	
0.741 3	0.734 3	0.723 3	0.736 3	0.689 3	0.664 3	0.644 3).609 3	1.610 4	1.601 4	0.625 3	0.642 3	0.687 3	0.705 3	0.730 3	0.769 2	0.806 2	0.795 2	0.808 2	0.800 2	0.792 2	0.776 2	0.774 3	0.747 3	RHmix T		
32.3 0.1	33.6 0.	34.9 0.	36.0 0.1	37.2 0.	38.2 0.	39.0 0.	39.6 0.	40.0 0.	40.2 0.	39.6 0.	38.2 0.	36.1 0.	33.6 0.	31.2 0.	29.1 0.	27.6 0.1	27.2 0.	27.2 0.	27.6 0.	28.2 0.1	29.1 0.	30.0 0.	31.2 0.	Tmix W	90%	
0.003 0.7	0.003 0.7	0.003 0.7	0.003 0.7	0.003 0.8	0.003 0.8	0.003 0.6	0.003 0.6	0.003 0.5	0.003 0.6	0.003 0.5	0.003 0.8	0.003 0.8	0.003 0.6	0.003 0.6	0.002 0.7	0.002 0.7	0.002 0.7	0.002 0.7	0.002 0.7	0.002 0.7	0.002 0.7	0.003 0.7	0.003 0.7	Wmix RH	90% OA	
0.713 27	0.711 28	0.703 30	0.725 31	0.669 33	0.640 34	0.618 36	0.575 36	0.578 36	.567 36	0.596 36	0.612 34	0.661 31	0.673 29	0.694 26	0.742 24	0.789 23	0.772 21	0.790 2:	0.781 23	0.770 23	0.752 24	0.751 26	0.718 28	RHmix Tr		
27.6 0.0	29.0 0.0	30.4 0.0	1.7 0.0	33.0 0.0	34.2 0.0	35.0 0.0	35.7 0.0	36.1 0.0	36.3 0.0	35.7 0.0	34.2 0.0	31.7 0.0	29.0 0.0	26.3 0.0	24.0 0.0	22.3 0.0	21.9 0.0	21.9 0.0	22.4 0.0	23.1 0.0	24.0 0.0	25.0 0.0	26.3 0.0	Tmix Wr	100%	
0.002 0.6	0.002 0.8	0.002 0.8	0.003 0.8	0.002 0.8	0.002 0.5	0.002 0.5	0.002 0.5	0.002 0.5	0.002 0.5	0.002 0.5	0.002 0.5	0.002 0.8	0.002 0.8	0.002 0.8	0.002 0.8	0.002 0.7	0.002 0.8	0.002 0.7	0.002 0.7	0.002 0.6	0.002 0.6	0.002 0.6	0.002 0.6	Wmix RH	100% OA	
0.664	0.665	0.660	0.692	0.624	0.593	0.568	.517	0.523	0.509	0.544	0.557	0.607	0.615	0.627	0.670	0.717	0.687	0.713	0.705	0.699	0.683	0.693	0.659	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	00	7	8	5	4	3	2	_	Hour		
71.6	71.9	72.0	72.2	72.4	72.5	72.5	72.E	72.5	72.4	72.2	71.8	71.7	71.4	71.1	70.9	70.8	70.7	70.8	70.8	70.9	71.1	71.3	71.4	Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	2 0.009	0.009	7 0.009	0.009	0.009	0.009	0.009	7 0.009	0.009	0.009	0.009	0.009	0.009	0.009	× Wmix	Minimum OA	
9 0.542	9 0.540	9 0.538	9 0.536	9 0.533	9 0.530	9 0.529	9 0.527	9 0.527	9 0.528	9 0.530	9 0.534	9 0.538	9 0.542	9 0.545	9 0.549	9 0.552	9 0.551	9 0.551	9 0.550	9 0.549	9 0.548	9 0.546	9 0.544	ix RHmix	n OA	
2 71.5	0 71.7	8 71.	6 72.	3 72.	0 72.	9 72.	7 72.	7 72.	8 72.	0 72.1	71.8	8 71.5	2 71.	5 71.1	9 70.7	2 70.6	1 70.6	1 70.6	0 70.7	9 70.8	8 70.1	6 71.1	4 71.3	iix Tmix		
5 0.009	7 0.009	300.00	1 0.009	3 0.009	4 0.009	5 0.009	5 0.009	4 0.009	3 0.009	1 0.009	8 0.009	5 0.009	2 0.009	0.009	7 0.009	3 0.009	3 0.009	3 0.009	7 0.009	8 0.009	0.009	1 0.009	3 0.009	× Wmix	10% OA	
9 0.543	19 0.54	19 0.539	19 0.537	19 0.534	19 0.53	19 0.529	19 0.527	19 0.527	19 0.529	19 0.53	19 0.534	19 0.538	19 0.543	19 0.546	19 0.550	9 0.553	19 0.553	19 0.552	19 0.552	9 0.550	9 0.549	9 0.547	19 0.545	ix RHmix	OA	
3 68.0	1 68.4	9.88	7 69.2	4 69.5	1 69.8	9.69.6	7 69.9	7 69.8	9 69.6	1 69.2	4 68.6	8 68.0	3 67.5	9.88	0 66.5	3 66.2	3 66.1	2 66.2	2 66.3	0 66.5	9 66.8	7 67.2	5 67.6	ix Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	< Wmix	20% OA	
8 0.572	8 0.567	8 0.562	8 0.558	8 0.55	8 0.548	8 0.542	8 0.538	8 0.538	8 0.540	8 0.545	8 0.552	8 0.561	8 0.570	8 0.577	8 0.585	8 0.592	8 0.591	8 0.590	8 0.589	8 0.585	8 0.583	8 0.578	8 0.576	× RHmix)A	
84.5	65.2	65.8	8 66.3	8.83	67.1	87.4	8 67.4	87.3	66.9	66.2	85.5	64.6	63.7	62.9	62.2	61.8	61.7	61.8	62.0	62.3	62.8	63.3	63.9	× Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	0.008	Wmix	30% OA	
0.600	0.592	0.585	0.579	0.568	0.559	0.553	0.547	0.546	0.550	0.557	0.568	0.581	0.595	0.608	0.620	0.631	0.630	0.628	0.626	0.621	0.617	0.610	0.606	RHmix	Ą	
61.0	61.9	62.7	63.4	64.0	64.5	64.8	64.9	64.7	64.2	63.3	62.3	61.1	59.9	58.9	58.0	57.4	57.3	57.4	57.6	58.1	58.7	59.4	60.2	Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	40% OA	
0.628	0.618	0.607	0.599	0.584	0.572	0.563	0.554	0.553	0.558	0.568	0.581	0.600	0.620	0.637	0.654	0.671	0.669	0.665	0.663	0.655	0.650	0.641	0.636	RHmix	,	
57.6	58.6	59.6	60.5	61.3	61.9	62.3	62.4	62.1	61.5	60.4	59.1	57.6	56.1	54.8	53.7	53.0	52.8	52.9	53.3	53.8	54.6	55.5	58.5	Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	Wmix	50% OA	March
0.655	0.642	0.628	0.618	0.599	0.582	0.570	0.559	0.557	0.563	0.575	0.592	0.615	0.641	0.663	0.686	0.709	0.705	0.700	0.698	0.688	0.682	0.670	0.664	RHmix		
54.1	55.3	56.6	57.6	58.6	59.3	59.7	59.8	59.5	58.8	57.5	55.9	54.1	52.4	50.8	49.5	48.6	48.4	48.5	48.9	49.6	50.5	51.6	52.8	Tmix		
0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.006	0.006	Wmix	60% OA	
0.680	0.664	0.648	0.636	0.611	0.591	0.578	0.561	0.558	0.585	0.578	0.598	0.627	0.658	0.684	0.714	0.743	0.738	0.731	0.729	0.717	0.710	0.696	0.690	RHmix		
50.6	52.1	53.5	54.8	55.8	56.7	57.2	57.3	56.9	56.0	54.6	52.7	50.6	48.6	46.7	45.2	44.2	44.0	44.1	44.6	45.4	46.4	47.7	49.1	Tmix	7	
0.005	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	Wmix	70% OA	
0.702	0.684	0.665	0.652	0.622	0.597	0.578	0.560	0.555	0.563	0.577	0.599	0.632	899.0	0.699	0.735	0.772	0.764	0.755	0.754	0.739	0.733	0.717	0.713	RHmix		
47.1	48.8	50.4	51.9	53.1	54.0	54.6	54.8	54.4	53.3	51.7	49.6	47.1	44.8	42.7	41.0	39.8	39.5	39.7	40.3	41.1	42.4	43.8	45.4	Tmix	8	
0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.005	Wmix I	80% OA	
0.720	0.701	0.680	0.665	0.629	0.599	0.577	0.554	0.548	0.555	0.570	0.593	0.629	0.670	0.704	0.746	0.792	0.780	0.768	0.769	0.752	0.748	0.732	0.730	RHmix		
43.6	45.5	47.3	49.0	50.3	51.4	52.1	52.2	51.8	50.6	48.7	46.4	43.7	41.0	38.7	36.7	35.4	35.1	35.3	35.9	36.9	38.3	39.9	41.7	Tmix 1	91	
0.004	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.004	0.004	0.004	Wmix F	90% OA	
0.732	0.712	0.689	0.674	0.632	0.597	0.570	0.543	0.534	0.541	0.555	0.578	0.616	0.659	0.695	0.742	0.797	0.779	0.764	0.769	0.751	0.751	0.736	0.740	RHmix		
40.1 0	42.2 0	44.3 0	46.1 0	47.6 0	48.8 0	49.5 0	49.7 0	49.2 0	47.9 0	45.8 0	43.2 0	40.2 0	37.3 0	34.6 0	32.5 0	31.0 0	30.7 0	30.9 0	31.6 0	32.7 0	34.2 0	36.0 0	38.0 0	Tmix V	100	
0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.003 0	0.004 0	Wmix R	100% OA	
0.736	0.717	0.693	0.679	0.629	0.589	0.559	0.525	0.514	0.519	0.531	0.552	0.589	0.633	0.867	0.717	0.785	0.762	0.742	0.749	0.730	0.738	0.725	0.738	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	00	7	6	5	4	ω	2	1	Hour		
72.6	72.8	72.9	73.1	73.2	73.3	73.4	73.4	73.4	73.3	73.1	72.8	72.E	72.3	72.1	71.9	71.7	71.7	71.7	71.8	71.9	72.0	72.2	72.4	Tmix		
0.009	0.00	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	< Wmix	Minimum	
9 0.536	9 0.534	9 0.533	9 0.530	9 0.528	9 0.525	9 0.524	9 0.523	9 0.523	9 0.523	9 0.524	9 0.526	9 0.530	9 0.532	9 0.535	9 0.539	9 0.543	9 0.543	9 0.542	9 0.543	9 0.543	9 0.54	9 0.539	9 0.538	× RHmix	1 OA	
3 72.5	4 72.7	3 72.9	73.0	3 73.2	73.3	73.4	3 73.4	3 73.3	3 73.2	73.0	3 72.8	72.5	2 72.2	5 71.8	B 71.7	3 71.6	3 71.E	2 71.E	3 71.7	3 71.8	71.9	3 72.1	8 72.3	ix Tmix		
0.009	0.000	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	: Wmix	10% OA	
0.537	0.534	0.533	0.531	0.528	0.526	0.524	0.523	0.523	0.524	0.524	0.527	0.530	0.533	0.536	0.539	0.544	0.544	0.544	0.544	0.544	0.542	0.540	0.538	< RHmix)A	
69.9	70.3	70.7	71.1	71.3	71.6	71.7	71.7	71.6	71.4	71.0	70.5	69.9	69.4	68.9	68.5	68.2	68.1	68.2	68.3	68.5	68.8	69.2	69.5	× Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.009	0.009	0.009	Wmix	20% OA	
0.558	0.554	0.551	0.546	0.540	0.536	0.532	0.530	0.531	0.531	0.532	0.537	0.544	0.549	0.555	0.563	0.572	0.573	0.572	0.573	0.573	0.568	0.564	0.562	RHmix	10	
67.4	68.0	68.6	69.1	69.5	8.83	70.1	70.1	70.0	69.6	69.0	68.3	67.4	66.6	65.8	65.2	64.8	64.7	64.8	65.0	65.3	65.7	66.3	8.88	Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	30% OA	
0.580	0.573	0.569	0.561	0.553	0.545	0.540	0.537	0.538	0.537	0.540	0.546	0.557	0.584	0.574	0.586	0.602	0.603	0.601	0.603	0.602	0.595	0.589	0.586	RHmix		
64.9	65.7	66.4	67.1	67.7	68.1	68.4	68.5	68.3	67.8	67.0	0.88	64.9	63.8	62.8	62.0	61.4	61.3	61.4	61.6	62.0	62.6	63.3	64.1	Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	0.008	0.008	Wmix	40% OA	
0.602	0.592	0.587	0.576	0.564	0.555	0.547	0.542	0.544	0.543	0.546	0.554	0.568	0.578	0.591	0.609	0.631	0.633	0.630	0.633	0.633	0.623	0.614	0.610	RHmix		
62.3	63.3	64.3	65.2	65.9	66.4	66.8	66.9	66.6	66.0	65.0	63.8	62.3	61.0	59.7	58.7	58.0	57.9	58.0	58.3	58.8	59.6	60.4	61.3	Tmix		
0.007	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	50% OA	April
0.624	0.612	909.0	0.590	0.576	0.563	0.553	0.548	0.549	0.548	0.550	0.561	0.578	0.590	0.606	0.629	0.659	0.662	0.658	0.663	0.663	0.650	0.639	0.633	RHmix		
59.8	61.0	62.2	63.2	64.0	64.7	65.1	65.2	64.9	64.2	63.0	61.5	59.8	58.2	56.7	55.5	54.7	54.4	54.5	54.9	55.5	56.5	57.5	58.6	Tmix	9	
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.007	0.007	0.007	Wmix	60% OA	
0.646	0.631	0.624	0.605	0.587	0.572	0.559	0.552	0.553	0.551	0.553	0.585	0.586	0.599	0.619	0.648	0.687	0.690	0.684	0.692	0.693	0.677	0.663	0.657	RHmix		
57.3	58.7	60.0	61.2	62.2	63.0	63.5	63.6	63.3	62.4	61.0	59.3	57.3	55.4	53.6	52.2	51.3	51.0	51.1	51.6	52.3	53.4	54.6	55.8	Tmix	7	
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.005	0.005	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	Wmix F	70% OA	
0.668	0.649	0.642	0.619	0.598	0.579	0.563	0.555	0.557	0.553	0.555	0.567	0.591	0.605	0.627	0.663	0.713	0.717	0.709	0.720	0.722	0.702	0.687	0.680	RHmix		
54.7	56.3	57.9	59.2	60.4	61.3	61.8	62.0	61.6	60.6	59.0	57.0	54.8	52.6	50.6	49.0	47.9	47.6	47.7	48.3	49.1	50.3	51.7	53.1	Tmix	81	
0.006	0.006	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.008	0.008	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.006	0.006	0.006	Wmix F	80% OA	
0.689	0.668	0.660	0.633	809.0	0.586	0.587	0.557	0.558	0.554	0.554	0.587	0.594	0.607	0.632	0.674	0.735	0.740	0.730	0.745	0.750	0.726	0.709	0.703	RHmix		
52.2	54.0	55.7	57.3	58.5	59.5	60.2	60.3	59.9	58.8	57.0	54.8	52.2	49.8	47.5	45.7	44.5	44.1	44.3	44.9	45.8	47.2	48.8	50.4	Tmix 1	91	
0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.004	0.004	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	Wmix F	90% OA	
0.708	0.685	0.677	.646	0.617	0.591	0.570	0.558	0.580	0.553	0.550	0.563	0.592	0.604	0.630	0.679	0.753	0.758	0.747	0.767	0.775	0.748	0.728	0.723	RHmix		
49.7 0	51.7 0	53.6 0	55.3 0	56.7 0	57.8 0	58.5	58.7 0	58.2 0	57.0 0	55.0 0	52.5 0	49.7 0	47.0 0	44.5	42.5 0	41.1	40.7 0	40.9 0	41.6 0	42.6 0	44.1	45.8 0	47.6 0	Tmix V	10.	
0.005 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.005 0	0.005 0	0.005 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.005 0	0.005 0	0.005 0	0.005 0	Wmix R	00% OA	
0.727	3.701	0.693	0.659	0.625	0.598	0.571	0.558	0.559	0.549	0.544	0.555	0.585	0.594	0.620	0.675	0.765	0.770	0.758	0.784	0.796	0.766	0.745	0.742	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	00	7	6	5	4	3	2	1	Hour		
73.8	74.1	74.4	74.6	74.9	75.1	75.2	75.2	75.2	75.1	74.9	74.6	74.4	74.1	73.8	73.5	73.2	73.0	72.9	72.9	72.9	73.0	73.2	73.5	Tmix		
0.009	0.009	0.008	0.008	0.008	0.008	0.009	0.008	0.008	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	Minimum	
0.521	0.520	0.518	0.515	0.511	0.508	0.506	0.505	0.506	0.507	0.508	0.510	0.513	0.517	0.520	0.524	0.529	0.532	0.533	0.533	0.532	0.530	0.528	0.525	RHmix	OA	
73.7	74.0	74.3	74.6	74.9	75.1	75.2	75.2	75.2	75.1	74.9	74.6	74.3	74.0	73.7	73.4	73.2	73.0	72.8	72.8	72.8	73.0	73.2	73.4	× Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	10% OA	
0.522	0.520	0.518	0.515	0.511	0.507	0.508	0.505	0.505	0.507	0.508	0.510	0.513	0.517	0.520	0.524	0.529	0.533	0.534	0.534	0.533	0.531	0.528	0.526	RHmix	A	
72.4	73.0	73.7	74.2	74.8	75.1	75.4	75.5	75.4	75.1	74.8	74.3	73.7	73.0	72.4	71.8	71.3	70.9	70.7	70.6	70.7	70.9	71.3	71.8	Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	20% OA	
0.527	0.525	0.520	0.514	0.505	0.499	0.496	0.494	0.495	0.498	0.501	0.505	0.509	0.517	0.524	0.533	0.543	0.550	0.552	0.552	0.550	0.546	0.540	0.535	RHmix		
71.1	72.1	73.0	73.9	74.6	75.2	75.6	75.7	75.6	75.2	74.6	73.9	73.0	72.1	71.1	70.2	69.5	6.83	68.5	68.4	68.5	6.88	69.5	70.2	Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.009	Wmix	30% OA	
0.533	0.529	0.522	0.513	0.500	0.491	0.486	0.483	0.485	0.489	0.493	0.499	0.505	0.518	0.528	0.541	0.558	0.568	0.571	0.571	0.587	0.561	0.552	0.545	RHmix		
69.9	71.1	72.3	73.5	74.5	75.3	75.7	75.9	75.7	75.3	74.5	73.5	72.3	71.1	69.9	68.7	67.6	66.9	66.4	66.2	66.4	66.9	67.6	9.89	Tmix		
0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	40% OA	
0.538	0.533	0.524	0.512	0.495	0.483	0.476	0.473	0.475	0.480	0.485	0.493	0.501	0.518	0.531	0.548	0.570	0.586	0.590	0.590	0.584	0.576	0.584	0.554	RHmix		
68.6	70.1	71.7	73.1	74.4	75.3	75.9	76.1	75.9	75.3	74.4	73.1	71.7	70.1	68.6	67.1	65.8	64.8	64.2	64.0	64.2	64.8	65.8	67.1	Tmix		
0.008	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	50% OA	May
0.542	0.537	0.525	0.511	0.490	0.475	0.467	0.463	0.465	0.471	0.478	0.486	0.497	0.517	0.533	0.555	0.583	0.604	0.610	0.609	0.602	0.590	0.576	0.563	RHmix		
67.3	69.1	71.0	72.7	74.3	75.4	76.1	76.4	76.1	75.4	74.3	72.8	71.0	69.1	67.3	65.5	64.0	62.8	62.1	61.8	62.1	62.8	64.0	65.5	Tmix	6	
0.008	0.008	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.007	0.008	0.008	0.007	0.007	0.007	0.007	0.007	800.0	Wmix	60% OA	
0.547	0.540	0.527	0.510	0.484	0.467	0.457	0.452	0.455	0.463	0.470	0.480	0.492	0.516	0.535	0.562	0.596	0.622	0.629	0.629	0.619	0.604	0.587	0.571	RHmix		
66.0	68.2	70.3	72.4	74.1	75.5	76.3	76.6	76.3	75.5	74.1	72.4	70.3	68.2	66.0	63.9	62.1	8.08	59.9	59.7	59.9	8.08	62.1	63.9	Tmix	71	
0.007	0.008	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix F	70% OA	
0.550	0.544	0.528	0.508	0.479	0.459	0.448	0.442	0.445	0.454	0.462	0.473	0.486	0.514	0.536	0.568	0.609	0.641	0.648	0.648	0.636	0.618	0.597	0.579	RHmix		
64.7	67.2	69.7	72.0	74.0	75.5	76.5	76.8	76.5	75.5	74.0	72.0	69.7	67.2	64.7	62.3	60.3	58.7	57.8	57.5	57.8	58.8	60.3	62.3	Tmix 1	80	
0.007 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.008 (0.007 (0.007 (0.007 (0.007 (0.007 (0.007 (0.007 (0.007 (0.007 (0.007 (0.007 (0.007 (Wmix F	80% OA	
0.553	0.547	0.529	0.507	0.474	0.451	0.438	0.432	0.435	0.445	0.454	0.486	0.480	0.512	0.537	0.573	0.622	0.659	0.667	0.666	0.652	0.631	0.607	0.586	RHmix		
63.4 (66.2 0	69.0 0	71.6 0	73.9 0	75.6 0	76.7 0	77.0 0	76.7 0	75.6 (73.9 (71.6 0	69.0 0	66.2 (63.4 (60.7 (58.4 (56.7 (55.6 (55.3 (55.6 (56.7 (58.5 (60.7 (Tmix \	90	
0.007 (0.008 0	0.008 0	0.008 (0.008 0	0.008 0	0.008 0	0.008 (0.008 0	0.008 (0.008 0	0.008 0	0.007 0	0.007 0	0.007 0	0.006 (0.007 0	0.007 0	0.006 (0.006 0	0.006 0	0.006 (0.006 0	0.007 (Wmix F	90% OA	
0.558 6	0.550 6	0.531 8	0.505	0.468	0.443	0.429	0.422	0.426	0.437	0.446	0.459	0.474 8	0.509 8	0.536 6	0.577 8	0.633 6	0.677 5	989.0	0.685	0.667	0.644 6	0.616 6	0.593 6	RHmix		
62.1 0	65.2 0	68.3 0	71.2 0	73.8 0	75.6 0	76.9 0	77.3 0	76.9 0	75.6 0	73.8 0	71.3 0	68.4 0	65.2 0	62.1 0	59.1 0	56.6 0	54.7 0	53.5 0	53.1 0	53.5 0	54.7 0	56.6 0	59.1 0	Tmix V	101	
0.007 0	0.007 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.008 0	0.007 0	0.007 0	0.007 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	Wmix R	100% OA	
0.558	0.552	0.531	0.504	0.463	0.435	0.420	0.413	0.416	0.428	0.438	0.452	0.467	0.506	0.535	0.580	0.644	0.694	0.704	0.702	0.682	0.655	0.624	0.599	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	8	5	4	3	2	1	Hour		
74.5	74.7	75.0	75.2	75.3	75.5	75.6	75.6	75.6	75.4	75.3	75.0	74.8	74.5	74.2	74.0	73.8	73.7	73.7	73.7	73.8	73.9	74.1	74.3	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.01	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.010	0.010	0.010	0.009	0.010	0.010	0.010	: Wmix	Minimum OA	
0.534	0.533	0.531	0.529	0.522	0.517	0.516	0.514	0.514	0.51	0.518	0.519	0.521	0.523	0.526	0.531	0.534	0.538	0.538	0.538	0.535	0.534	0.534	0.536	x RHmix	1 OA	
74.5	8 74.7	75.0	75.2	2 75.4	75.5	75.6	75.6	75.6	75.5	75.3	75.0	74.8	74.5	8 74.2	74.0	73.8	8 73.7	73.6	73.6	5 73.7	73.9	74.0	8 74.3	ix Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.010	0.010	0.010	0.009	0.010	0.010	0.010	Wmix	10% OA	
0.535	0.534	0.532	0.529	0.522	0.517	0.515	0.514	0.514	0.517	0.518	0.520	0.521	0.523	0.526	0.531	0.535	0.539	0.539	0.539	0.536	0.535	0.535	0.536	: RHmix	A	
74.0	74.5	74.9	75.4	75.7	76.0	76.2	76.2	76.2	75.9	75.6	75.1	74.5	73.9	73.4	72.9	72.5	72.3	72.2	72.3	72.5	72.7	73.1	73.5	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.010	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	20% OA	
0.555	0.552	0.548	0.542	0.529	0.518	0.515	0.512	0.512	0.518	0.520	0.524	0.527	0.531	0.538	0.547	0.555	0.564	0.564	0.563	0.558	0.554	0.555	0.558	RHmix	4	
73.5	74.2	74.9	75.5	76.1	76.5	76.8	76.8	76.7	76.4	75.8	75.1	74.3	73.4	72.6	71.9	71.3	71.0	70.8	70.9	71.2	71.6	72.1	72.8	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.010	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	30% OA	
0.576	0.570	0.565	0.556	0.535	0.519	0.514	0.511	0.510	0.519	0.522	0.528	0.532	0.540	0.549	0.564	0.576	0.590	0.590	0.588	0.580	0.575	0.576	0.580	RHmix	1	
73.0	73.9	74.9	75.7	76.5	77.0	77.3	77.5	77.3	76.8	76.1	75.1	74.1	72.9	71.8	70.8	70.1	69.6	69.4	69.5	69.9	70.5	71.2	72.0	Tmix		
0.010	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.010	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	40% OA	
0.597	0.589	0.581	0.569	0.541	0.520	0.513	0.509	0.507	0.520	0.523	0.531	0.538	0.548	0.561	0.581	0.598	0.617	0.617	0.615	0.604	0.597	0.598	0.603	RHmix		
72.4	73.7	74.9	75.9	76.8	77.5	77.9	78.1	77.9	77.3	76.4	75.2	73.8	72.4	71.0	69.8	8.88	68.3	68.1	68.2	68.6	69.3	70.2	71.3	Tmix		
0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	50% OA	June
0.619	0.608	0.598	0.581	0.546	0.521	0.513	0.507	0.505	0.521	0.525	0.535	0.544	0.558	0.573	0.599	0.621	0.646	0.646	0.643	0.628	0.619	0.621	0.627	RHmix		
71.9	73.4	74.8	76.1	77.2	78.0	78.5	78.7	78.5	77.7	76.7	75.2	73.6	71.8	70.2	8.88	67.6	66.9	66.7	8.88	67.4	68.2	69.3	5.07	Tmix		
0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.011	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	60% OA	
0.641	0.627	0.614	0.594	0.552	0.521	0.512	0.505	0.503	0.521	0.527	0.539	0.550	0.585	0.585	0.617	0.645	0.676	0.676	0.673	0.654	0.642	0.644	0.652	RHmix		
71.4	73.1	74.8	76.3	77.5	78.5	79.1	79.3	79.0	78.2	76.9	75.2	73.3	71.3	69.4	67.7	66.4	65.6	65.3	65.4	66.1	67.1	68.3	8.83	Tmix		
0.011	0.011	0.012	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.010	0.011	Wmix	70% OA	
0.664	0.647	0.631	0.606	0.557	0.522	0.511	0.503	0.501	0.522	0.528	0.543	0.555	0.573	0.597	0.636	0.670	0.708	0.708	0.704	0.681	0.867	0.669	0.678	RHmix		
70.9	72.8	74.8	76.5	77.9	79.0	79.7	79.9	79.6	78.6	77.2	75.3	73.1	70.8	68.6	66.7	65.1	64.2	63.9	64.1	64.8	65.9	67.4	69.1	Tmix		
0.011	0.011	0.012	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.010	0.011	Wmix	80% OA	
0.688	0.666	0.647	0.619	0.562	0.522	0.509	0.501	0.498	0.522	0.530	0.547	0.561	0.582	0.610	0.656	0.696	0.741	0.741	0.737	0.710	0.692	0.694	0.704	RHmix		
70.4	72.6	74.7	76.6	78.3	79.5	80.3	80.5	80.2	79.1	77.5	75.3	72.9	70.3	67.8	65.6	63.9	62.9	62.5	62.7	63.5	64.8	66.4	68.3	Tmix	9	
0.011	0.012	0.012	0.012	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.010	0.011	Wmix	90% OA	
0.712	0.687	0.664	0.631	0.567	0.522	0.508	0.498	0.496	0.523	0.531	0.551	0.567	0.591	0.623	0.676	0.724	0.777	0.777	0.772	0.739	0.719	0.721	0.732	RHmix		
69.9	72.3	74.7	76.8	78.6	80.0	80.9	81.1	80.8	79.5	77.8	75.3	72.6	69.7	67.0	64.6	62.7	61.5	61.1	61.3	62.3	63.7	65.5	67.6	Tmix	10	
0.011	0.012	0.013	0.013	0.012	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.010	0.011	Wmix F	100% OA	
0.736	0.707	0.680	0.643	0.572	0.522	0.507	0.496	0.493	0.523	0.533	0.555	0.573	0.600	0.637	0.698	0.752	0.814	0.814	808.0	0.771	0.748	0.748	0.760	RHmix		

	23	22	21 7	20 7	19 7	18	17	16	15 7	14	13	12	11	10	9	8	7	6	5	4	ω	2	1	T non		
7/7 0	74.9 0	75.1 0	75.3 0	75.4 0	75.6 0	75.7 0	75.9 0	75.9 0	75.9 0	75.9 0	75.8 0	75.6 0	75.3 0	75.1 0	74.8 0	74.5 0	74.3 0	74.2 0	74.2 0.	74.2 0	74.3 0.	74.4 0.	74.5 0	īmi× ∀	Minimum	
010 0	.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	0.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	010 0.	.010 0.	.010 0.	.010 0.	.010 0.	.010 0.	0.010 0.	Wmix RH	num OA	
537 74	.537 74	.534 75.	.533 75	.529 75.	.525 75	.520 75	.520 75	.520 76.	.522 78.	.525 75	.527 75	.530 75	.533 75	.536 75.	.538 74	.543 74	.547 74	.545 74	.543 74	.542 74.	.540 74	.540 74	0.538 74	RHmix Tr		
17 0010	1.9 0.010	5.1 0.010	5.3 0.010	5.5 0.010	5.6 0.010	5.8 0.010	5.9 0.010	3.0 0.010	3.0 0.010	5.9 0.010	5.8 0.010	5.6 0.010	5.3 0.010	5.1 0.010	1.8 0.010	1.5 0.010	1.3 0.010	1.2 0.010	1.1 0.010	1.2 0.010	1.2 0.010	1.4 0.010	1.5 0.010	Tmix Wmix	10%	
110 0.538	110 0.538	110 0.535	110 0.534	110 0.530	110 0.525	110 0.520	110 0.520	110 0.520	110 0.523	110 0.525	110 0.528	110 0.530	110 0.533	110 0.537	110 0.539	110 0.545	110 0.548	110 0.546	110 0.544	110 0.543	110 0.541	110 0.541	110 0.539	nix RHmix	0% OA	
743	74.7	75.1	75.5	75.9	76.3	76.6	76.8	76.9	77.0	76.9	76.6	76.2	75.7	75.1	74.6	74.0	73.6	73.4	73.3	73.3	73.5	73.7	74.0	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	Wmix	20% OA	
0.580	0.560	0.554	0.552	0.544	0.534	0.524	0.524	0.524	0.529	0.533	0.539	0.544	0.550	0.557	0.563	0.574	0.581	0.577	0.573	0.572	0.568	0.566	0.563	RHmix		
74.0	74.6	75.2	75.8	76.4	76.9	77.3	77.7	77.9	77.9	77.8	77.4	76.8	76.0	75.2	74.4	73.6	72.9	72.6	72.4	72.5	72.7	73.1	73.5	Tmix		
0.010	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	Wmix	30% OA	
0.583	0.583	0.573	0.570	0.557	0.542	0.527	0.527	0.527	0.534	0.541	0.549	0.557	0.567	0.578	0.587	0.605	0.616	0.610	0.604	0.602	0.596	0.593	0.587	RHmix		
73.7	74.4	75.3	76.1	76.9	77.5	78.1	78.5	78.8	78.9	78.7	78.2	77.4	76.4	75.3	74.2	73.1	72.3	71.7	71.6	71.7	72.0	72.4	73.0	Tmix	41	
0.011	0.011 (0.011 (0.011 (0.011 (0.011 (0.011 (0.011 (0.011 (0.011 (0.011 (0.012 (0.011 (0.011 0	0.011 (0.011 (0.011 0	0.011 (0.011 (0.010 (0.010 (0.010 (0.011 (0.011 (Wmix F	40% OA	
0.607	0.605	0.592	0.587	0.570	0.549	0.530	0.529	0.530	0.538	3.547	0.558	0.570	0.583	0.598	0.611	.636	0.652	0.644	0.636	0.633	0.624	0.620	0.612	RHmix		
73.3 0	74.3 0	75.4 0	76.4 0	77.3 0	78.2 0	78.9 0	79.4 0	79.8 0	79.9 0	79.7 0	79.0 0	78.0 0	76.7 0	75.4 0	73.9 0	72.6 0	71.6 0	70.9 0	70.7 0	70.9 0	71.2 0	71.8 0	72.5 0	Tmix V	50	
0.011 0	.011 0.	.011 0.	.012 0.	.012 0.).011 0.	.011 0.	.011 0.).012 0.	.012 0.).012 0.	.012 0.	.012 0.	.012 0.	.012 0.	.011 0.	.011 0.	.011 0.	.011 0.	.011 0.	.011 0.	.011 0.	0.011 0.	0.011 0.	Wmix RI	50% OA	July
630 7	.628 7.	.611 7	.604 7	.582 7	0.556 7	.532 7	.531 8	.532 8	.542 8	.553 8	.587 7	.582 7	.599 7	.619 7	0.636 7	.668 7	.689 7	0.679 7	0.669 6	.665 7	0.654 7	0.649 7	0.638 7	RHmix Ti		
73.0 0.0	74.2 0.01	75.4 0.1	1.0 9.97	77.8 0.1	1.0 8.87	79.7 0.1	80.3 0.1	1.0 7.08	1.0 6.08	1.0 9.08	79.8 0.1	1.0 9.87	77.1 0.1	75.4 O.I	73.7 0.0	72.1 O.I	1.0 6.02	70.1 O.I	0.0	1.0 0.07	70.5 0.1	71.1 0.0	72.0 0.011	Tmix W	60%	
.011 0.655	2 0	1.012 0.630	.012 0.6).012 0.594	1.012 0.563).012 0.6	.012 0.6	.012 0.5	.012 0.545	1.012 0.559	.013 0.575	1.012 0.593	.012 0.614	.012 0.639	.012 0.8).012 0.701	.012 0.727	.011 0.716	.011 0.704	.011 0.6	.011 0.685	0.678	0.664	Wmix RH	6 OA	
72.	.651 74.	30 75.	.621 76.	94 78.	63 79.).534 80.	0.533 81	.534 81.7	645 81	59 81	75 80.	93 79.	814 77.	39 75.	.661 73.	71 71	70.	16 69.	704 69.	.699 69.	85 69.	878 70.	71	RHmix Tmix		
.7 0.0	.0 0.0	.5 0.0	.9 0.0	.2 0.0	.4 0.0	.4 0.0	.2 0.0	.7 0.0	0.0	.5 0.0	0.0	.2 0.0	.4 0.0	.5 0.0	.5 0.0	.7 0.0	.2 0.0	.3 0.0	0.0	.2 0.0	.7 0.0	.5 0.0	.5 0.0	nix Wmi:	70%	
12 0.67	12 0.675	12 0.648	13 0.637	13 0.606	12 0.569	12 0.536	12 0.534	12 0.535	13 0.548	13 0.563	13 0.582	13 0.604	13 0.629	12 0.659	12 0.686	12 0.735	12 0.767	12 0.754	11 0.740	11 0.73	11 0.717	11 0.708	11 0.691	iix RHmix	OA	
79 724	5 73.9	8 75.6	77.2	6 78.7	9 80.1	81.2	82.1	5 82.6	8 82.8	3 82.5	2 81.4	79.8	9 77.7	9 75.6	6 73.3	5 71.2	7 69.5	4 68.5	0 68.2	4 68.4	7 68.9	8.69	11 71.0	iix Tmix		
0.012	0.012	0.013	0.013	0.013	0.013	0.012	0.013	0.013	0.013	0.013	0.014	0.013	0.013	0.013	0.012	0.013	0.012	0.012	0.011	0.011	0.011	0.012	0.012	< Wmix	80% OA	
0.704	0.698	0.667	0.653	0.617	0.575	0.537	0.535	0.536	0.550	0.567	0.589	0.614	0.644	0.680	0.712	0.770	0.809	0.794	0.778	0.771	0.750	0.740	0.719	RHmix)A	
72.0	73.7	75.6	77.5	79.2	80.7	82.0	83.0	83.6	83.8	83.4	82.2	80.4	78.1	75.6	73.1	70.7	8.88	67.7	67.3	67.5	68.2	69.2	70.5	Tmix		
0.012	0.013	0.013	0.013	0.013	0.013	0.013	0.013	0.013	0.014	0.014	0.014	0.014	0.014	0.013	0.013	0.013	0.013	0.012	0.012	0.012	0.012	0.012	0.012	Wmix	90% OA	
0.730	0.722	0.685	0.669	0.627	0.580	0.539	0.536	0.536	0.552	0.570	0.595	0.623	0.658	0.699	0.737	0.805	0.852	0.836	0.817	0.809	0.785	0.772	0.748	RHmix		
717	73.6	75.7	77.7	79.6	81.3	82.8	83.9	84.5	84.8	84.3	83.0	81.0	78.4	75.7	72.9	70.2	68.1	66.9	66.5	66.7	67.4	68.5	70.0	Tmix	1	
0.013	0.013	0.013	0.014	0.014	0.013	0.013	0.013	0.014	0.014	0.014	0.015	0.014	0.014	0.014	0.013	0.013	0.013	0.012	0.012	0.012	0.012	0.012	0.012	Wmix	100% OA	
0.758	0.746	0.704	0.684	0.637	0.585	0.539	0.536	0.536	0.553	0.573	0.600	0.632	0.672	0.719	0.764	0.842	0.896	0.879	0.858	0.848	0.821	0.805	0.777	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	00	7	6	5	4	3	2	1	Hour		
74.4	74.6	74.8	75.0	75.2	75.4	75.5	75.6	75.6	75.6	75.4	75.2	74.9	74.6	74.3	74.0	73.8	73.6	73.6	73.6	73.7	73.8	74.0	74.2	Tmix	M	
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.010	0.010	0.010	VVmix	Minimum (
0.534	0.533	0.533	0.529	0.525	0.519	0.517	0.515	0.516	0.517	0.517	0.519	0.522	0.524	0.529	0.533	0.537	0.539	0.537	0.536	0.537	0.535	0.535	0.534	RHmix	OA	
74.4	74.6	74.8	75.1	75.3	75.4	75.5	75.6	75.6	75.6	75.4	75.2	74.9	74.6	74.3	74.0	73.7	73.6	73.5	73.6	73.6	73.8	73.9	74.1	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.010	0.010	0.010	Wmix	10% OA	
0.535	0.534	0.533	0.530	0.525	0.519	0.517	0.515	0.516	0.517	0.518	0.519	0.522	0.525	0.529	0.534	0.538	0.540	0.538	0.537	0.537	0.536	0.536	0.535	RHmix		
73.7	74.2	74.7	75.1	75.5	75.8	76.1	76.3	76.3	76.2	75.9	75.4	74.8	74.2	73.5	73.0	72.5	72.2	72.1	72.1	72.3	72.5	72.9	73.3	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	20% OA	
0.555	0.553	0.551	0.544	0.534	0.523	0.518	0.515	0.517	0.517	0.519	0.522	0.529	0.534	0.543	0.552	0.561	0.585	0.562	0.560	0.560	0.557	0.556	0.555	RHmix		
73.1	73.8	74.5	75.2	75.8	76.2	76.6	76.9	76.9	76.8	76.3	75.6	74.8	73.8	72.8	71.9	71.2	70.8	70.6	70.7	70.9	71.3	71.8	72.4	Tmix		
0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	30% OA	
0.575	0.572	0.569	0.559	0.544	0.526	0.519	0.514	0.517	0.518	0.521	0.526	0.535	0.544	0.558	0.572	0.585	0.592	0.587	0.583	0.584	0.580	0.578	0.576	RHmix		
72.4	73.4	74.3	75.2	76.0	76.7	77.2	77.5	77.6	77.4	76.8	75.9	74.7	73.4	72.1	70.9	70.0	69.4	69.2	69.3	69.6	70.1	70.8	71.6	Tmix	4	
0.010	0.010	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	40% OA	
0.596	0.592	0.587	0.573	0.552	0.529	0.519	0.513	0.517	0.518	0.522	0.529	0.542	0.553	0.572	0.592	0.611	0.620	0.613	809.0	0.609	0.603	0.600	0.598	RHmix		
71.8	73.0	74.2	75.3	76.3	77.1	77.7	78.1	78.2	78.0	77.2	76.1	74.6	73.0	71.4	69.9	68.7	0.89	67.7	67.8	68.2	8.88	69.7	70.7	Tmix	5	
0.010	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix	50% OA	August
0.618	0.612	0.605	0.587	0.561	0.532	0.520	0.512	0.517	0.518	0.524	0.532	0.548	0.563	0.588	0.613	0.637	0.649	0.640	0.634	0.636	0.627	0.624	0.620	RHmix		
71.2	72.5	74.0	75.3	76.5	77.5	78.3	78.8	78.9	78.6	77.7	76.3	74.5	72.6	70.6	68.9	67.5	66.5	66.3	66.4	9.33	67.6	68.6	8.88	Tmix	- 6	
0.010	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.010	0.010	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.010	0.010	Wmix F	60% OA	
0.640	0.632	0.624	0.601	0.570	0.535	0.520	0.511	0.516	0.518	0.525	0.535	0.555	0.573	0.603	0.635	0.665	0.681	0.669	0.662	0.663	0.653	0.649	0.644	RHmix		
70.5 0	72.1 (73.8 (75.4 (76.8 (77.9 (78.8 (79.4 (79.5 (79.2 (78.1 (76.5 (74.5	72.2 (69.9	67.9 (66.2	65.1 (64.8	65.0 (65.5	66.4 (67.6	69.0 0	Tmix \	70	
.011	0.011 (0.011 (0.012 (0.011 (0.011 (0.011 (0.011 (0.011 (0.011 (0.011 0	0.010 (0.010 0	0.010 (0.010 (0.010 (0.010 (0.009 (0.009 (0.009 (0.009 (0.009 (0.010 (.010	Wmix F	70% OA	
0.663	0.653	0.642	0.615	0.578	0.537	0.521	0.510	0.516	0.518	0.526	0.538	0.562	0.584	0.620	0.657	0.695	0.714	0.699	0.691	0.692	0.679	0.674	899.0	RHmix		
69.9	71.7	73.7 (75.4 C	77.0 0	78.3 (79.4 (80.0 0	80.2 (79.8 (78.6 0	78.7 (74.4 [71.7 0	69.2 C	66.8 0	65.0 C	63.7 (63.3	63.5	64.2	65.1 C	66.5	68.1 (Tmix V	80	
0.011 0	0.011 0	0.012 0	0.012 0	0.012 0	0.011 0	0.011 0	0.011 0	0.011 0	0.011 0	0.011 0	0.011 0	0.010 0	0.010 0	0.010 0	0.010 0	0.010 0	0.009 0	0.009 0	0.009 0	0.009 0	0.009 0	0.010 0	0.010 0	Wmix R	80% OA	
0.687 6	0.674	0.661	0.629	0.586	0.540	0.521	0.509 8	0.515	0.518 8	0.527	0.541	0.568	0.594	0.636 6	0.681 6	0.726 8	0.748 6	0.731 6	0.721 6	0.723 6	0.707 6	0.701 6	0.693 6	RHmix 7		
69.2 0	71.3 0	73.5 0	75.5 0	77.3 0	78.7 0	79.9 0	80.6 0	80.8 0	80.4 0	79.0 0	76.9 0	74.3 0	71.3 0	68.4 0	65.8 0	63.7 0	62.3 0	61.9 0	62.1 0	62.8 0	63.9 0	65.4 0	67.2 0	Tmix V	90	
0.011 0	0.011 0	0.012 0	0.012 0	0.012 0	0.011 0	0.011 0	0.011 0	0.012 0	0.011 0	0.011 0	0.011 0	0.010 0	0.010 0	0.010 0	0.010 0	0.010 0	0.009 0	0.009 0	0.009 0	0.009 0	0.009 0	0.010 0	0.010 0	Wmix RI	90% OA	
0.712 6	0.696 7	0.680 7	0.643 7).594 7	0.542 7).521 8	.507 8	0.514 8	0.518 8	1.528 7	0.544 7	0.575 7	0.605 7	0.653 6	0.706 6	0.758 6	0.785 6	0.765 6	0.753 6	0.755 6	0.737 6	0.729 6	0.719 6	RHmix T		
68.6	70.9 0.	73.3 0.	75.5 0.	77.5 0.	79.1 0.	80.5 0.	81.3 0.	81.5 0.	81.0 0.	79.5 0.	77.1 0.	74.2 0.	70.9 0.	67.7 0.	64.8 0.	62.4 0.	60.9 0.	60.4 0.	60.6 0.	61.4 0.	62.7 0.	64.4 0.	66.4 0.	Tmix W	100	
0.011 0.	0.012 0.	0.012 0.	0.012 0.	0.012 0.	0.012 0.	0.012 0.	0.012 0.	0.012 0.	0.012 0.	0.011 0.	0.011 0.	0.010 0.	0.010 0.	0.010 0.	0.010 0.	0.010 0.	0.009 0.	0.009 0.	0.009 0.	0.009 0.	0.009 0.	0.010 0.	0.010 0.	Wmix RH	00% OA	
0.737	0.718	0.699	0.657	0.602	0.544	0.521	0.506	0.513	0.517	0.528	0.547	0.582	0.615	0.671	0.731	0.792	0.824	0.801	0.786	0.789	0.767	0.758	0.747	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	00	7	9	5	4	з	2	-	Hour		
73.9	74.1	74.3	74.6	74.8	74.9	75.1	75.2	75.2	75.3	75.2	74.9	74.6	74.1	73.7	73.3	73.1	73.0	73.0	73.1	73.2	73.3	73.5	73.7	Tmix		
0.008	0.000	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	VVmix	Minimum	
0.530	0.529	0.527	0.525	0.521	0.518	0.509	0.507	0.508	0.507	0.510	0.512	0.517	0.521	0.525	0.531	0.536	0.538	0.538	0.538	0.536	0.535	0.533	0.531	RHmix	OA	
73.9	74.1	74.3	74.5	74.7	74.9	75.1	75.2	75.2	75.3	75.2	74.9	74.5	74.1	73.6	73.3	73.0	72.9	72.9	73.0	73.1	73.3	73.4	73.6	× Tmix		
0.009	0.009	0.010	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	10% OA	
0.531	0.530	0.528	0.525	0.522	0.516	0.509	0.507	0.507	0.507	0.510	0.512	0.517	0.521	0.525	0.531	0.537	0.539	0.539	0.538	0.537	0.536	0.533	0.532	RHmix	A	
72.7	73.2	73.6	74.1	74.5	74.8	75.1	75.4	75.5	75.5	75.4	74.9	74.1	73.2	72.3	71.5	71.0	70.8	70.8	71.0	71.2	71.5	71.9	72.3	Tmix		
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	20% OA	
0.547	0.544	0.540	0.535	0.528	0.516	0.502	0.498	0.499	0.498	0.504	0.508	0.518	0.527	0.535	0.547	0.559	0.564	0.563	0.562	0.559	0.558	0.552	0.548	RHmix	1	
71.6	72.3	73.0	73.6	74.2	74.8	75.2	75.5	75.7	75.8	75.5	74.8	73.6	72.3	70.9	8.83	69.0	68.7	8.83	69.0	69.3	8.89	70.3	70.9	mix		
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	30% OA	
0.564	0.559	0.553	0.545	0.534	0.516	0.495	0.489	0.491	0.489	0.498	0.504	0.519	0.533	0.545	0.563	0.582	0.590	0.588	0.587	0.582	0.580	0.571	0.565	RHmix		
70.4	71.4	72.3	73.2	74.0	74.7	75.3	75.7	76.0	76.1	75.7	74.7	73.2	71.4	69.6	0.88	67.0	66.6	66.7	67.0	67.4	0.88	68.7	9.69	Tmix		
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	40% OA	
0.581	0.574	0.566	0.555	0.540	0.516	0.488	0.480	0.483	0.481	0.492	0.500	0.520	0.538	0.554	0.579	0.606	0.618	0.615	0.613	0.606	0.604	0.591	0.583	RHmix		
69.3	70.5	71.6	72.7	73.7	74.6	75.3	75.9	76.2	76.3	75.9	74.6	72.7	70.5	68.2	66.3	65.0	64.5	64.6	65.0	65.5	66.3	67.1	68.2	Tmix		Si
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.009	0.009	0.009	Wmix	50% OA	September
0.598	0.589	0.579	0.566	0.547	0.516	0.482	0.471	0.475	0.473	0.486	0.496	0.521	0.544	0.564	0.598	0.630	0.647	0.643	0.641	0.631	0.628	0.612	0.601	RHmix		r
68.2	69.5	70.9	72.3	73.5	74.5	75.4	76.1	76.5	76.6	76.1	74.6	72.3	69.6	66.9	64.6	63.0	62.4	62.5	63.0	63.6	64.5	65.6	8.88	Tmix	6	
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	800.0	0.008	800.0	0.008	0.008	0.009	Wmix	60% OA	
0.617	0.606	0.593	0.576	0.553	0.516	0.475	0.463	0.467	0.464	0.481	0.492	0.522	0.549	0.573	0.613	0.656	0.677	0.672	0.670	0.657	0.654	0.633	0.620	RHmix		
67.0	68.6	70.3	71.8	73.2	74.5	75.5	76.2	76.7	76.9	76.2	74.5	71.8	68.7	65.5	62.8	61.0	60.3	60.5	80.9	61.7	62.8	64.0	65.5	Tmix	7	
0.009	0.009	0.010	0.010	0.010	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.009	Wmix F	70% OA	
0.636	0.622	0.607	0.587	0.580	0.516	0.468	0.454	0.460	0.456	0.475	0.488	0.523	0.554	0.582	0.630	0.683	0.709	0.702	0.700	0.685	0.681	0.655	0.639	RHmix		
65.9	67.7	69.6	71.3	73.0	74.4	75.5	76.4	77.0	77.1	76.4	74.4	71.4	67.7	64.1	61.1	59.0	58.2	58.4	58.9	59.8	61.0	62.4	64.1	Tmix 1	80	
0.009 (0.009 0	0.010 0	0.010 0	0.010 0	0.009 0	0.009 0	0.009 0	0.009 0	0.009 (0.009 0	0.009 0	0.009 0	0.008 0	0.008 0	0.007 0	0.008 0	0.008 0	0.008 0	0.008 (0.008 0	0.008 (0.008 0	0.008 (Wmix F	80% OA	
0.655	0.640	0.621	0.598	0.566	0.516	0.461	0.446	0.452	0.448	0.470	0.484	0.524	0.560	1.592	0.648	0.711	0.742	0.734	0.731	0.713	0.709	0.678	0.659	RHmix		
64.7 (8.88	6.88	70.9 0	72.7	74.3 (75.6 (76.6 (77.2	77.4 (76.6 (74.3 (70.9 (66.8 0	62.8 0	59.3 (56.9 0	56.1 (56.3 (56.9 (57.9 0	59.3 (60.9 0	62.8 0	Tmix \	90	
0.009 0	0.009 0	0.010 0	0.010 0	0.010 0	0.009 0	0.009 0	0.009 0	0.009 0	0.009 (0.009 0	0.009 0	0.008 0	0.008 0	0.007 0	0.007 0	0.007 0	0.007 0	0.007 0	0.008 (0.008 0	0.008 0	0.008 0	0.008 0	Wmix F	90% OA	
1.676 6	0.657 6	0.636 6	0.609	0.573	0.516	0.455	0.437	0.445	0.440	0.464	0.480	0.525	0.565 6	0.600 6	0.665 6	0.740 6	0.777 8	0.767 6	0.764 5	0.743 6	0.738 8	0.702 6	0.680 6	RHmix		
63.6 0	65.9 0	68.2 0	70.4 0	72.4 0	74.2 0	75.6 0	76.8 0	77.5 0	77.6 0	76.8 0	74.3 0	70.4 0	65.9 0	61.4 0	57.6 0	54.9 0	54.0 0	54.2 0	54.9 0	56.1 0	57.6 0	59.3 0	61.4 0	Tmix V	10:	
0.009 0	0.009 0	0.010 0	0.010 0	0.010 0	0.009 0	0.008 0	0.008 0	0.009 0	0.009 0	0.009 0	0.009 0	0.008 0	0.008 0	0.007 0	0.007 0	0.007 0	0.007 0	0.007 0	0.007 0	0.007 0	0.008 0	0.008 0	0.008 0	Wmix R	100% OA	
0.697	0.676	0.652	0.621	0.580	0.516	0.448	0.429	0.437	0.432	0.459	0.476	0.525	0.570	0.609	0.682	0.769	0.813	0.802	0.799	0.774	0.769	0.727	0.702	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	80	7	8	5	4	3	2	1	Hour		
72.6	72.9	73.1	73.3	73.4	73.6	73.7	73.8	73.8	73.7	73.6	73.3	72.9	72.6	72.2	71.9	71.7	71.7	71.7	71.8	71.9	72.0	72.2	72.4	Tmix		
0.009	0.000	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	Minimum	
0.536	0.534	0.532	0.530	0.528	0.523	0.517	0.516	0.515	0.516	0.518	0.520	0.525	0.531	0.536	0.541	0.545	0.545	0.545	0.544	0.543	0.542	0.540	0.539	RHmix	OA	
72.5	72.8	73.0	73.2	73.4	73.5	73.7	73.7	73.7	73.7	73.5	73.2	72.8	72.5	72.1	71.8	71.6	71.5	71.6	71.6	71.8	71.9	72.1	72.3	× Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	Wmix	10% OA	
0.537	0.535	0.532	0.530	0.528	0.523	0.517	0.516	0.515	0.516	0.518	0.521	0.525	0.531	0.537	0.542	0.546	0.546	0.546	0.545	0.544	0.543	0.541	0.540	RHmix	A	
70.1	70.5	71.0	71.4	71.8	72.1	72.3	72.4	72.5	72.4	72.0	71.4	70.7	69.9	69.2	68.6	68.2	68.1	68.1	68.3	68.5	8.88	69.2	69.6	Tmix		
0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.009	0.009	0.009	0.009	Wmix	20% OA	
0.558	0.554	0.549	0.545	0.541	0.531	0.518	0.515	0.513	0.516	0.520	0.525	0.534	0.546	0.558	0.568	0.577	0.578	0.578	0.575	0.574	0.571	0.567	0.585	RHmix		
67.6	68.3	69.0	69.6	70.1	70.6	71.0	71.2	71.2	71.1	70.5	69.6	68.5	67.4	66.3	65.4	64.8	64.6	64.7	64.9	65.3	65.7	66.3	66.9	Tmix		
0.008	0.008	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	30% OA	
0.580	0.575	0.567	0.560	0.554	0.538	0.518	0.514	0.510	0.515	0.521	0.527	0.542	0.561	0.579	0.595	0.609	0.611	0.610	909.0	0.605	0.601	0.594	0.590	RHmix		
65.1	66.1	67.0	67.8	68.5	69.2	89.8	69.9	70.0	69.7	69.0	67.8	66.4	64.8	63.4	62.2	61.4	61.2	61.3	61.5	62.0	62.6	63.4	64.2	Tmix	- 4	
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.008	0.008	0.008	0.008	Wmix	40% OA	
0.603	0.595	0.584	0.575	0.567	0.545	0.518	0.512	0.508	0.513	0.521	0.529	0.548	0.574	0.599	0.622	0.642	0.644	0.644	0.638	0.636	0.630	0.622	0.617	RHmix		
62.7	63.8	64.9	66.0	66.9	67.7	68.3	68.6	68.7	68.4	67.5	66.0	64.2	62.3	60.5	59.0	58.0	57.7	57.8	58.2	58.8	59.5	60.5	61.5	Tmix	5	0
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix F	50% OA	October
0.626	0.615	0.602	0.590	0.580	0.551	0.516	0.508	0.501	0.509	0.519	0.529	0.553	0.586	0.619	0.649	0.675	0.678	0.677	0.670	0.667	0.661	0.650	0.643	RHmix		
60.2 (61.6	62.9 (64.2	65.3	66.3 (66.9 0	67.3 (67.5	67.1 (66.0 0	64.2 0	62.1 0	59.8 0	57.6 0	55.8 0	54.6 0	54.3 0	54.4 (54.8 0	55.5 0	56.4 0	57.5 0	58.8 (Tmix \	60	
0.007 (0.007 (0.008 (0.008 (0.008 (0.008 0	0.007 (0.007 (0.007 (0.007 (.007 (.007	.007	.006	.006	.006	.006	.006	0.006 (.006	.007	.007	.007	0.007 (Wmix F	60% OA	
0.648	0.636	0.620	0.605	0.593	0.557	0.513	0.504	0.495	0.505	0.517	0.528	0.556	0.596	0.636	0.675	0.708	0.712	0.711	0.701	0.699	0.691	0.678	0.670	RHmix		
57.8 0	59.4 0	60.9 0	62.4 0	63.7 0	64.8 0	65.6 0	66.1 0	66.2 0	65.8 0	64.5	62.4 0	59.9 0	57.2 0	54.7 0	52.6 0	51.2 0	50.8 0	50.9 0	51.5 0	52.3 0	53.4 0	54.6 0	56.1 0	Tmix V	70	
.007 (.007 0	.007 0	.007 0	.008 0	.007 0	.007 0	.007 0	.007 0	.007 0	.007 0	.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	.006 0	.007	Wmix R	70% OA	
1.671 6	0.657 6	0.637 6	0.620 8	9 509.0	0.563 6	0.509 8	0.498 8	0.488 6	0.500 8	0.513 8	0.524 8	0.557 6	0.604 6	0.652 6	0.699 4	0.740 4	0.744 4	0.743 4	0.731 4	0.730 4	0.721 6	0.705 6	0.697 6	RHmix 1		
55.3 0	57.1 0	58.9 0	60.6 0	62.0 0	63.3 0	64.2 0	64.8 0	65.0 0	64.5 0	63.0 0	0 9.09	57.7 0	54.7 0	51.8 0	49.4 0	47.8 0	47.4 0	47.5 0	48.1 0	49.0 0	50.3 0	51.7 0	53.4 0	Tmix V	80	
0.006 0	0.007 0	0.007 0	0.007 0	0.007 0	0.007 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.006 0	0.005 0	0.005 0	0.005 0	0.005 0	0.005 0	0.005 0	0.006 0	0.006 0	0.006 0	0.006 0	Wmix R	80% OA	
0.693 5	0.678 5	0.655 5	0.635 5	0.618 6	0.567 6	0.504 8	0.492 6	0.479 8	0.493 6	0.507 8	0.518 5	0.554 5	0.609 5	0.665 4	0.720 4	0.770 4	0.775 4	0.774 4	0.760 4	0.760 4	0.750 4	0.732 4	0.724 5	RHmix T		
52.8 0.	54.9 0.	56.9 0.	58.8 0.	60.4 0.	61.9 0.	62.9 0.	63.5 0.	63.7 0.	63.2 0.	61.4 0.	58.8 0.	55.6 0.	52.1 0.	48.9 0.	46.2 0.	44.4 0.	43.9 0.	44.1 0.	44.7 0.	45.8 0.	47.2 0.	48.8 0.	50.7 0.	Tmix W	909	
0.006 0.	0.006 0.	0.007 0.	0.007 0.	0.007 0.	0.007 0.	0.006 0.	0.006 0.	0.006 0.	0.006 0.	0.006 0.	0.005 0.	0.005 0.	0.005 0.	0.005 0.	0.005 0.	0.005 0.	0.005 0.	0.005 0.	0.005 0.	0.005 0.	0.005 0.	0.006 0.	0.006 0.	Wmix RH	90% OA	
0.715 5	0.698 5	0.672 5	0.649 5	0.631 5	0.571 6	0.498 6	0.483 6	0.469 6	0.484 6	0.500 5	0.510 5	.549 5).611 4	0.674 4	0.738 4	0.798 4	0.803 4).802 4	0.785 4	0.787 4	0.778 4	0.758 4	0.751 4	RHmix Ti		
50.4 0.0	52.7 0.1	54.9 0.1	57.0 0.1	58.8 0.0	60.4 0.1	61.5 0.0	62.2 0.1	62.4 0.1	61.8 0.1	59.9 0.0	57.0 0.1	53.4 0.1	49.6 0.1	46.0 0.1	43.0 0.0	41.0 0.1	40.4 0.1	40.6 0.1	41.4 0.1	42.6 O.I	44.1 0.1	45.9 0.1	48.0 0.1	Tmix W	100	
0.006 0.3	0.006 0.3	0.006 0.6	0.007 0.6	0.007 0.6	0.006 0.5	0.006 0.4	0.006 0.4	0.005 0.4	0.006 0.4	0.005 0.4	0.005 0.4	0.005 0.5	0.005 0.6	0.004 0.6	0.004 0.3	0.004 0.8	0.004 0.8	0.004 0.8	0.004 0.8	0.005 0.8	0.005 0.8	0.005 0.3	0.005 0.3	Wmix RH	100% OA	
0.736	0.718	0.689	0.664	0.643	0.574	0.490	0.474	0.457	0.474	0.490	0.499	0.540	0.608	0.678	0.751	0.821	0.826	0.826	0.806	0.811	0.803	0.782	0.778	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	00	7	8	5	4	ω	2	_	Hour		
72.0	72.2	72.5	72.7	72.8	73.0	73.1	73.2	73.2	73.1	72.9	72.7	72.3	72.0	71.6	71.3	71.1	71.1	71.1	71.2	71.3	71.4	71.6	71.8	Tmix		
0.00	0.00	0.009	0.000	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	: Wmix	Minimum	
9 0.539	9 0.537	9 0.535	9 0.535	9 0.532	9 0.529	9 0.525	9 0.522	9 0.521	9 0.522	9 0.524	9 0.528	9 0.532	9 0.536	9 0.542	9 0.546	9 0.548	9 0.548	9 0.549	9 0.548	9 0.547	9 0.545	9 0.543	9 0.541	× RHmix	1 OA	
9 71.8	7 72.	5 72.4	5 72.6	2 72.7	9 72.9	5 73.0	2 73.	1 73.	2 73.0	4 72.9	8 72.8	2 72.3	6 71.8	2 71.5	6 71.3	8 71.0	8 70.9	9 71.0	8 71.0	7 71.	5 71.3	3 71.5	1 71.	ix Tmix		
0.00	0.00	0.009	0.009	7 0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	2 0.009	8 0.009	5 0.009	2 0.009	0.009	0.009	0.009	0.009	0.009	0.009	5 0.009	7 0.009	< Wmix	10% OA	
9 0.540	9 0.538	9 0.536	9 0.535	9 0.533	9 0.530	9 0.526	9 0.523	9 0.52	9 0.522	9 0.524	9 0.528	9 0.532	9 0.537	9 0.543	9 0.547	9 0.550	9 0.549	9 0.550	9 0.549	9 0.548	9 0.546	9 0.544	9 0.542	× RHmix)A	
68.8	69.3	69.7	70.1	70.5	70.8	71.0	71.2	71.2	2 71.1	70.7	70.1	69.4	68.7	68.0	67.4	67.0	66.9	66.9	87.1	87.3	67.6	68.0	88.4	x Tmix		
0.008	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	20% OA	
0.584	0.560	0.556	0.555	0.550	0.544	0.535	0.529	0.525	0.527	0.532	0.540	0.548	0.559	0.570	0.579	0.585	0.584	0.585	0.583	0.581	0.578	0.574	0.569	: RHmix)A	
65.7	66.4	67.1	67.7	68.2	68.7	69.0	69.2	69.3	69.1	68.6	67.7	66.6	65.5	64.5	63.6	63.0	62.8	62.9	63.1	63.4	63.9	64.4	65.0	< Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	Wmix	30% OA	
0.588	0.583	0.575	0.575	0.567	0.558	0.544	0.533	0.529	0.531	0.538	0.550	0.563	0.579	0.596	0.612	0.620	0.619	0.621	0.618	0.615	0.610	0.604	0.596	RHmix	Д	
62.6	63.5	64.4	65.2	0.88	8.88	67.0	67.3	67.4	67.2	66.4	65.2	63.8	62.4	60.9	59.8	59.0	58.7	58.8	59.1	59.5	60.2	60.9	61.7	Tmix		
0.007	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	40% OA	
0.612	0.605	0.595	0.595	0.585	0.571	0.552	0.537	0.530	0.534	0.543	0.559	0.576	0.598	0.622	0.645	0.656	0.653	0.657	0.652	0.649	0.642	0.633	0.623	RHmix		
59.5	60.7	61.8	62.8	63.7	64.5	65.1	65.4	65.5	65.2	64.3	62.8	61.1	59.2	57.4	55.9	55.0	54.7	54.8	55.1	55.7	56.4	57.4	58.4	Tmix		
0.007	0.007	0.007	0.007	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.007	0.007	Wmix	50% OA	November
0.635	0.626	0.614	0.616	0.602	0.584	0.559	0.539	0.530	0.535	0.548	0.566	0.587	0.616	0.647	0.676	0.691	0.686	0.693	0.685	0.682	0.673	0.662	0.649	RHmix		ñ
56.4	57.8	59.1	60.3	61.5	62.4	63.1	63.5	63.6	63.3	62.1	60.4	58.3	56.0	53.9	52.1	51.0	50.6	50.7	51.2	51.8	52.7	53.9	1.55	Tmix		
0.006	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	Wmix	60% OA	
0.657	0.647	0.633	0.635	0.618	0.596	0.565	0.540	0.529	0.534	0.547	0.571	0.596	0.630	0.669	0.705	0.723	0.716	0.726	0.717	0.713	0.703	0.689	0.674	RHmix		
53.3	55.0	56.5	57.9	59.2	60.3	61.1	61.6	61.7	61.3	60.0	57.9	55.5	52.9	50.4	48.3	47.0	46.6	46.7	47.2	48.0	49.0	50.4	51.8	Tmix		
0.006	0.006	0.006	0.007	0.007	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.006	0.006	Wmix	70% OA	
0.677	0.666	0.650	0.655	0.634	0.608	0.569	0.538	0.525	0.531	0.545	0.573	0.601	0.641	0.687	0.731	0.752	0.742	0.755	0.744	0.741	0.729	0.714	969.0	RHmix		
50.2	52.1	53.9	55.5	57.0	58.2	59.1	59.7	59.8	59.3	57.8	55.5	52.7	49.7	46.9	44.5	43.0	42.5	42.6	43.2	44.1	45.3	46.8	48.5	Tmix	8	
0.005	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.005	0.005	0.005	0.005	Wmix I	80% OA	
0.694	0.683	0.665	0.673	0.649	0.618	0.572	0.535	0.518	0.525	0.540	0.572	0.603	0.647	0.700	0.752	0.775	0.760	0.777	0.765	0.764	0.751	0.735	0.715	RHmix		
47.1	49.2	51.2	53.0	54.7	56.1	57.1	57.7	57.9	57.4	55.7	53.1	49.9	46.5	43.4	40.7	39.0	38.4	38.6	39.2	40.2	41.6	43.3	45.1	Tmix 1	91	
0.005	0.005	0.005	0.006	0.006	0.006	0.008	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.005	Wmix F	90% OA	
0.706	0.697	0.678	0.690	0.663	0.627	0.572	0.528	0.508	0.517	0.532	0.587	0.598	0.647	0.706	0.764	0.789	0.767	0.791	0.776	0.778	0.766	0.750	0.730	RHmix		
44.1	46.4 (48.6 0	50.6 (52.5 (54.0 (55.1 (55.8 (56.0 (55.4 (53.5	50.6 (47.1 (43.4 (39.8 (36.9 (35.0 0	34.4 (34.5	35.3 (36.4 (37.9 (39.8 (41.8 (Tmix \	10	
0.004 0	0.005 0	0.005 0	0.005 0	0.006 0	0.006 0	0.005 0	0.005 0	0.005 0	0.005 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.004 0	0.003 0	0.003 0	0.003 0	0.003 0	0.004 0	0.004 0	0.004 0	0.004 (Wmix R	100% OA	
0.714	1.707	0.688	0.706	0.676	0.634	0.570	0.519	0.496	0.505	0.520	0.557	0.588	0.638	0.702	0.766	0.790	0.759	0.790	0.775	0.782	0.772	0.757	0.738	RHmix		

24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	00	7	8	5	4	3	2	1	Hour		
71.0	71.1	71.2	71.3	71.4	71.5	71.6	71.8	71.8	71.8	71.5	71.3	71.1	70.9	70.7	70.6	70.4	70.4	70.4	70.5	70.5	70.6	70.7	70.8	Tmix		
0.009	0.009	2 0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	7 0.009	0.009	0.009	0.009	0.009	0.009	0.009	0.009	7 0.009	0.009	× Wmix	Minimum OA	
9 0.550	9 0.549	9 0.548	9 0.546	9 0.545	9 0.544	9 0.542	9 0.54	9 0.541	9 0.54	9 0.542	9 0.544	9 0.546	9 0.549	9 0.552	9 0.555	9 0.556	9 0.555	9 0.555	9 0.555	9 0.554	9 0.553	9 0.552	9 0.552	ix RHmix	n OA	
0 70.8	9 70.9	8 71.1	6 71.2	5 71.3	4 71.4	2 71.5	1 71.5	1 71.5	1 71.5	2 71.	4 71.2	6 71.0	9 70.8	2 70.6	5 70.4	6 70.3	5 70.2	5 70.2	5 70.3	4 70.4	3 70.4	2 70.6	2 70.7	iix Tmix		
3 0.009	9 0.00g	1 0.009	2 0.009	3 0.009	4 0.009	5 0.009	5 0.009	5 0.009	5 0.009	4 0.009	2 0.009	300.0	8 0.009	3 0.009	4 0.009	3 0.009	2 0.009	2 0.009	3 0.009	4 0.009	4 0.009	3 0.009	7 0.009	x Wmix	10% OA	
19 0.552	19 0.550	19 0.549	19 0.547	19 0.548	19 0.545	19 0.544	19 0.542	19 0.542	19 0.542	19 0.543	19 0.545	19 0.548	19 0.550	19 0.554	19 0.558	19 0.557	19 0.557	19 0.557	9 0.558	9 0.558	9 0.555	9 0.553	9 0.553	ix RHmix	OA .	
2 66.6	0 66.9	9 67.1	7 67.4	6 67.6	5 67.8	4 67.9	2 68.0	2 68.0	2 68.0	3 67.7	5 67.4	8 67.0	0 66.5	4 66.1	65.8	7 85.5	7 85.5	7 65.5	65.6	6 65.7	5 65.9	3 66.1	3 66.3	ix Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	< Wmix	20% OA	
0.589	8 0.586	0.584	8 0.580	8 0.577	8 0.575	8 0.572	8 0.569	8 0.568	8 0.569	8 0.571	8 0.575	8 0.580	8 0.586	0.593	0.598	0.600	0.600	0.600	0.598	8 0.597	0.595	0.592	0.592	< RHmix)A	
62.4	62.8	63.2	63.6	63.9	64.2	64.4	64.5	64.5	64.4	64.1	63.6	63.0	62.3	61.7	61.1	8.08	60.7	60.7	60.9	61.1	61.3	61.7	62.0	x Tmix		
0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.008	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	30% OA	
0.628	0.623	0.619	0.613	0.608	0.605	0.600	0.595	0.593	0.595	0.599	0.605	0.612	0.622	0.634	0.642	0.645	0.644	0.643	0.641	0.640	0.636	0.632	0.631	RHmix	Ą	
58.2	58.7	59.3	59.7	60.2	8.08	8.08	61.0	61.1	60.9	60.5	59.8	59.0	58.1	57.2	58.5	56.1	55.9	56.0	56.2	56.4	56.8	57.2	57.7	Tmix		
0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	0.007	Wmix	40% OA	
0.666	0.660	0.654	0.646	0.639	0.635	0.628	0.621	0.617	0.620	0.625	0.634	0.644	0.657	0.674	0.685	0.690	0.688	0.687	0.684	0.682	0.677	0.671	0.671	RHmix	,	
54.0	54.7	55.3	55.9	58.5	56.9	57.3	57.5	57.6	57.4	56.8	56.0	55.0	53.8	52.8	51.9	51.3	51.2	51.2	51.5	51.8	52.2	52.8	53.4	Tmix]
0.006	0.006	0.006	0.006	0.006	0.007	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	Wmix	50% OA	December
0.704	0.695	0.689	0.678	0.669	0.664	0.654	0.645	0.640	0.643	0.650	0.661	0.673	0.690	0.713	0.728	0.733	0.730	0.729	0.725	0.723	0.716	0.708	0.710	RHmix		r
49.8	50.6	51.4	52.1	52.8	53.3	53.7	54.0	54.1	53.9	53.2	52.2	50.9	49.6	48.3	47.3	46.6	46.4	46.5	46.7	47.1	47.7	48.3	49.0	Tmix		
0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.006	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	Wmix	60% OA	
0.740	0.729	0.721	0.709	0.696	0.692	0.678	0.666	0.880	0.663	0.672	0.685	0.699	0.720	0.748	0.767	0.772	0.767	0.766	0.761	0.759	0.752	0.742	0.746	RHmix		
45.6	46.5	47.5	48.3	49.1	49.7	50.2	50.5	50.6	50.3	49.5	48.3	46.9	45.4	43.9	42.6	41.9	41.6	41.7	42.0	42.5	43.1	43.9	44.7	Tmix	7	
0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.005	0.005	0.005	Wmix	70% OA	
0.771	0.759	0.751	0.736	0.721	0.716	0.699	0.684	0.676	0.680	0.689	0.703	0.720	0.744	0.778	0.800	0.804	0.797	0.796	0.790	0.788	0.780	0.769	0.777	RHmix		
41.4	42.5	43.5	44.5	45.4	46.1	46.6	46.9	47.1	46.8	45.9	44.5	42.9	41.1	39.4	38.0	37.1	36.8	37.0	37.3	37.8	38.5	39.4	40.4	Tmix	8	
0.004	0.004	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.005	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	Wmix RHmix	80 % OA	
0.795	0.783	0.775	0.758	0.741	0.736	0.715	0.696	0.686	0.690	0.700	0.715	0.732	0.758	0.798	0.822	0.825	0.813	0.812	0.806	0.805	0.798	0.785	0.800	Н		
37.2	38.4	39.6	40.7	41.7	42.5	43.1	43.4	43.6	43.3	42.3	40.7	38.9	36.9	35.0	33.4	32.4	32.1	32.2	32.6	33.2	34.0	35.0	36.0	Tmix	9	
0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.004	Wmix F	90% OA	
0.809	0.797	0.791	0.772	0.753	0.749	0.724	0.701	0.689	0.693	0.703	0.717	0.733	0.759	0.803	0.828	0.826	0.809	0.809	0.802	0.804	0.798	0.787	0.811	RHmix		
33.0 (34.3 (35.7 (36.9 (38.0 0	38.9 (39.5	39.9 (40.1 (39.8 (38.6 (36.9 (34.9 (32.7 (30.5 0	28.8 (27.7 (27.3 (27.5 (27.9 (28.5 (29.4 (30.5 0	31.7 0	Tmix \	10	
0.003 (0.003 (0.003 (0.004 0	0.004 (0.004 0	0.004 0	0.004 0	0.004 0	0.004 (0.003 (0.003 0	0.003 (0.003 0	0.003 (0.003 (0.003 0	0.002 (0.002 (0.002 (0.003 (0.003 (0.003 (0.003 0	Wmix F	100% OA	
0.807	0.797	0.795	0.775	0.755	0.753	0.723	0.695	0.681	0.685	0.694	0.708	0.717	0.740	0.793	0.824	0.819	0.793	0.795	0.786	0.791	0.785	0.771	0.805	RHmix		